

Adsorption mechanism and modelling of hydrocarbon contaminants onto rice straw activated carbons

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The adsorption of Diphenolic acid (DPA), 2,4-Dichlorophenoxyacetic acid (2,4-D), and 2-methyl-4-chlorophenoxyacetic acid (MCPA) were examined in aqueous solution using activated carbon rice straw. The rice straw was activated by using two reagents, zinc chloride and phosphoric acid and named as RSZ, RSP, respectively. The results showed that both carbons have a relatively high adsorption capacity. Concerning the adsorption kinetic, the second-order model has better fit than the first model to experimental data. The adsorption yield of both carbons increased in the order: DPA < 2,4-D < MCPA. The pore volume diffusion model satisfactorily fitted the experiment on both carbons. Furthermore, solution pH has a high influence on the adsorption capacity for both carbons. The adsorption mechanism of selected pollutants onto carbon samples has been controlled by dispersion interaction π - π electrons and electrostatic interaction, moreover, the contribution of pore volume diffusion is the controlling mechanism of the overall rate of adsorption.

Keywords: Activated carbon, rice straw, adsorption mechanism, adsorption modeling, pore volume surface diffusion.

INTRODUCTION

Contamination of natural waters is a problem worldwide, which can have grave consequences on the health of both humans and animals¹. Large amounts and various organic hydrocarbons (e.g. pesticides, plasticizers) contaminate natural water sources and other natural resources. This is mostly due to the worsening unsustainable anthropogenic activities (industrial, urban, agricultural, farming, etc.)².

The novel effects of herbicides at significant concentrations in the environment was reported recently by Orton et al.³. Due to being low cost and of good selectivity⁴, 2,4-dichlorophenoxyacetic acid (2,4-D) is a broadly used herbicide⁵. Moreover, both in cultivated and non-cultivated application, 4-chloro-2-methylphenoxiacetic acid (MCPA) is frequently used to control a broad variety of broadleaf weeds⁶. Both compounds (2,4-D and MCPA) proved relatively pervasive in global drinking water sources⁷.

In the recent decade, it was observed that in order to synthesize new polyesters and polycarbonates, Diphenolic acid (DPA) was generally preferred over Bisphenol A (BPA)^{8, 9}. This is mainly due to DPA being more commercially available and much cheaper than BPA. As a result, DPA became the more abundant environmental pollutant than BPA. DPA is known to cause; a) severe endocrine system damage, b) carcinogenesis, c) liver damage and d) obesity-promoting¹⁰. DPA was also detected in various water systems¹¹.

Mailler et al.¹² examined the adsorption process of hydrocarbons on activated carbon and found a strong correlation between the absorption efficiency of activated carbons and their specific surface (BET). Ocampo-Pérez et al.¹³ examined the adsorption rates of 2,4-D, DPA and MCPA and other pollutants on two commercially activated carbons. They found that both diffusional and kinetic models successfully fit the experimental adsorption rate data. Abdel daiem et al.¹⁴ use of gamma radiation to oxidize DPA in aqueous solution proved to be an excellent option in removing DPA from aqueous solutions. The DPA degradation increases at higher irradiation doses but decreased in the presence of different anions in the aqueous solution. Rivera-Utrilla et al.¹⁵ studied the 2,4-D photodegradation by using UV/TiO₂ in the presence of different original and oxidized activated carbons. The results showed that the presence of ozonated activated carbons with a high carboxyl groups contents enhanced 2,4-D photodegradation by the UV/TiO₂ system, mineralized 40% of total organic carbon and reduced the toxicity of the degradation by-products. Tchaikovskaya et al.¹⁶ investigated the photodegradation of MCPA by UV radiation using KrCl and XeBr excilamps. They showed that by using excilamps caused the effective phototransformation of MCPA. Coupling of photo and bioprocess allow the removal of initial pollutant and photo products from water.

Activated carbon has been proven to be an effective adsorbent in aqueous media due to their highly developed porosity and surface area¹⁷. In recent years, the considerable attention of scientists has been devoted to preparing activated carbon materials from different agriculture biomass residues to help environmental protection^{18–20}.

Preparation of activated carbon from lignocellulose wastes is an effective method of solid waste recycle from the environmental point of view. Rice straw is considered to be one of the most important agriculture residues due to its high production worldwide, around 731 million tons/year²¹. Daifullah et al.¹⁸ investigated the preparation of activated carbon by one-step steam pyrolysis of rice straw at 550, 650, 750°C and modified

it by liquid-phase oxidation using HNO₃, H_2O_2 , and KMnO₄. They reported that the surface area of activated carbon samples ranged from 63 to 113 m²/g. Furthermore, Ahmedna et al.²² prepared activated carbons from rice straw by physical activation at 750°C and found their surface area less than 200 m²/g.

From this background, the main objectives of this study is thus established as: i) preparing activated carbon with optimally developed porosity and surface area from rice straw using zinc chloride and phosphoric acid, ii) studying the adsorption kinetics of 2,4-D, MCPA and DPA on prepared activated carbons by using diffusional and kinetic models, iii) analysing the influence of solution pH and ionic strength on adsorption yield to investigate the adsorption mechanism of selected pollutants in both activated carbons, iv) to study a selected pollutant adsorption process in a dynamic regime.

MATERIALS AND PREPARATION METHODOLOGY

Reagents

The chemical reagents utilized in this study are; 2,4-D, MCPA, DPA, zinc chloride, phosphoric acid, sodium chloride, sodium hydroxide and hydrochloric acid. All high-purity analytical grade reagents were supplied by Sigma–Aldrich. All the ultrapure water used were obtained from Milli-Q[®] equipment Millipore.

The concentrations of 2,4-D, DPA and MCPA were determined using UV-visible spectrophotometer (Genesys 5) at a wavelength of 284, 279 and 276 nm, respectively. The physic-chemical prosperities of these pollutants are presented in Table 1

Preparation of activated carbons

Two activated carbons were prepared from rice straw. They were obtained from Sevilla, Spain. The physical properties of rice straw used in this work showed that: ash content is 10.63%, volatile matter is 89.90%, carbon is 42.82%, hydrogen is 7.18% and nitrogen is $0.78\%^{23}$. The rice straw sample was shredded into a particle size of less than 4 mm then washed with distilled water to remove any impurities and dried at 110°C, overnight. The dried samples were mixed with $ZnCl_2$ or H_3PO_4 with impregnation ration (1:1) by weight (rice straw: activation agent) for two days at 60°C, and were designated as samples RSZ and RSP, respectively. The two samples were pyrolyzed under N₂ (flowrate = 300 cm^3 / min) at 300°C for 2 h and then at 800°C for 1 h at a heating rate of 10°C/min. The activated carbons obtained were then washed with distilled water to remove the phosphorous or zinc compounds until neutralization. The washed samples were then dried at 105°C for 24 h, finally obtaining the desired powder activated carbon. The activated carbon samples produced were chemically and texturally characterized. The methods and techniques used in characterization are detailed in²⁴⁻²⁶.

Adsorption kinetics and diffusion

The adsorption kinetics of the selected pollutants on the prepared activated carbons were observed by adding 100 mg of activated carbon sample in a 200 mL Erlenmeyer flasks containing 100 mg/L of selected pollutants. The flasks were then stored in a thermostatic mechanical shaker batch operating at a constant agitation speed of 135 rpm. The temperature was set at 298°K and the solution pH maintained at 3.20 (without any addition). The kinetic experiment resulted in a period to equilibrium of 7 days for DPA and 2,4-D and a period to

Pollutant	Molecular Weight [g/mol]	Molecular Size [nm]	Molecular formula	Maximal projection area [nm ²]	V _A ^{a)} [cm³/mol]	Solubility in water [g/L]	log K _{ow} ^{b)}	рК _{а1} с)	pK _{a2} d)	рК _{аз} е)
DPA	286.33	1.27 × 1.23 × 0.96		0.77	315	0.40	3.58	4.66	9.70	10.45
2,4-D	221.00	1.29 × 0.73 × 0.42		0.62	182	2.16	2.69	2.98	_	_
МСРА	200.62	1.24 × 0.84× 0.42		0.62	185	1.38	2.22	3.14	_	_

Table 1. Physical and chemical properties of the selected pollutants

a) Liquid molar volume at the standard boiling point.

b) Log octanol-water partition coefficient.

c, d, e) pK_a corresponding to the successive deprotonations.

equilibrium of 8 days for MCPA. The adsorption kinetic models commonly used are represented as the first- and second-order kinetic equations shown below:

$$q = q_{\text{pred},1} \left(1 - e^{-k_1 t} \right) \tag{1}$$

$$q = \frac{q_{\text{pred},2}^2 k_2 t}{1 + q_{\text{pred},2} k_2 t}$$
(2)

Moreover, the diffusion model is derived with the following assumptions: i) intraparticle diffusion (pore volume diffusion and surface diffusion), ii) the rate of adsorption on an active site is instantaneous, and iii) powder activated carbon particles are spherical. Choong et al.²⁷ and Leyva-Ramos and Geankoplis,²⁸ have described the model equations and its initial and boundary conditions by the following equations:

$$V\frac{dC_{A}}{dt} = -mSk_{L,exp}\left(C_{A} - C_{Ar}|_{r=R_{p}}\right)$$
(3)

$$t = 0, \quad C_A = C_{A0} \tag{4}$$

$$\varepsilon_{p} \frac{\partial C_{Ar}}{\partial t} + \rho_{p} \frac{\partial q}{\partial t} = \frac{1}{r^{2}} \frac{\partial}{\partial r} \left[r^{2} \left(D_{ep} \frac{\partial C_{Ar}}{\partial r} + D_{s} \rho_{p} \frac{\partial q}{\partial r} \right) \right]$$
(5)

$$C_{Ar} = 0, \quad t = 0, \quad 0 \le r \le R_p$$
 (6)

$$\frac{\partial C_{Ar}}{\partial t}\Big|_{r=0} = 0 \tag{7}$$

$$D_{ep} \frac{\partial C_{Ar}}{\partial r} \Big|_{r=R} + D_{s} \rho_{p} \frac{\partial q}{\partial r} = k_{L,exp} \left(C_{A} - C_{Ar} \Big|_{r=R_{p}} \right)$$
(8)

Three models examined in this study by applying the following models: (1) Pore volume surface diffusion model (PVSDM) which represented by equations (3–8), (2) Pore volume diffusion model (PVDM) by assuming ($D_{ep} \neq 0$, $D_s = 0$) and (3) Surface diffusion model (SDM) considering that ($D_{ep} = 0$, $D_s \neq 0$).

Matlab (software version 9.2) was used to numerically solve the coupled partial and ordinary differential equations of the three diffusion models. The *Matlab* code was based on finite difference scheme, forward time forward space (FTFS), of 2^{nd} order error approximation in both of time and space variables²⁹.

Adsorption Isotherm of Pollutants on Activated Carbons

Adsorption isotherms were derived using the same method to obtain adsorption kinetics. Varying concentrations of each pollutant (50, 100, 200, 300, 400, and 500 mg/L) was used. The effects of the solution pH was investigated initially at concentration 500 mg/L at varying solution pH values per flask (3 to 10) at 298°K. The working pH was derived by introducing varying volumes of HCl (50 mM) and NaOH (50 mM) into the solution. A CRISON micropH2002 meter was used to measure the solution pH.

The presence of electrolytes in the DPA, 2,4-D, and MCPA adsorption test solutions were analyzed at an initial concentration of 500 mg/L. The concentrations of NaCl (0.0 to 0.01 M) is then gradually increased. The ionic strengths of these derived solutions are similar to that of many types of water in nature³⁰. The solution pH is 3.20 (without any addition) at 298° K.

Adsorption process in dynamic regime

Adsorption was studied in a dynamic regime by passing a solution of 2,4-D, DPA or MCPA (200 mg/L) through a glass column (3.0 cm high and 1.0 cm diameter) filled with approximately 1.0 g of activated carbon samples. A peristaltic pump was used to pass the pollutant solutions through the active carbon beds at: a) a flow rate of 2.5 mL/ min, b) pH of 3.20 (without any addition) and c) 298°K. The techniques and methods used to derive the breakthrough curves are detailed in previous works^{30, 31}.

RESULT AND DISCUSSION

Characterization of activated carbons

The surface area of RSZ and RSP were determined by using nitrogen at 77°K which is considered as one of the most widely used techniques to assess textural properties of porous solids³². The textural characterization of prepared activated carbons is shown in Table 2. Both activated carbon samples used here have a bigger surface area compared to the ones used in Ahmedna et al.¹⁸. and Daifullah et al.²². Further, RSZ has a slightly bigger surface area (771 m²/g) than that for RSP (613 m²/g) due to the thermal treatment of the raw materials with ZnCl₂. This enhances the reaction of the chemical compound on the matrix of the precursors, fragmenting cellulose, hemicellulose and lignin which develop the pore structure upon activation³³.

The external surface area of carbon RSP (126 m²/g) proved to be larger than that of carbon RSZ (91 m²/g). Note that a sufficiently large collective volume of pores is available to the water being treated (> 0.40 cm³/g) for both activated carbons (Table 2). Micropore volume W_o (N₂) > W_o (CO₂), resulting into insignificant constrictions at the micropore entrances. Hence, complete accessibility to N₂ molecules at 77°K³⁴. L_o (N₂) for both activated carbon samples were larger than L_o (CO₂).

The chemical characteristic of the prepared activated carbons in Table 2 shows that in both carbons (RSZ and RSP) the ash content was very high – 39.68 and 48.26 respectively. The element analysis of carbon RSZ shows that Zn is the highest component followed by Si and Fe – 14.45%, 7.91% and 6.83%, respectively (Table 2). In RSP, P was the highest component followed by Si and Fe – 37.19%, 8.93%, and 5.77%, respectively (Table 2). This explains the higher ash content in RSP than RSZ. pH of the point of zero charge was 5.80 and 2.70 for RSZ and RSP, respectively. This means that RSZ is slightly acidic while RSP is strongly acidic.

Adsorption kinetic.

The adsorption kinetics of DPA, 2,4-D, and MCPA on RSZ and RSP were investigated using first-order and second-order kinetic models (eq. 1 and 2). The model constant (k_1 and k_2) were calculated by curve fitting the kinetic models into the experimental adsorption kinetic data curves. The model constants and their correlation coefficient (R^2) are given in Table 3. In general, the R^2 values for the first and second-order models are higher than 0.90. The only exceptions are: a) the k_1 in the adsorption kinetics of 2,4-D onto both activated carbons and b) DPA onto RSP – i.e. between 0.85 and 0.9. Evidently, the two kinetic models fit relatively well

with the experimental data (adsorption kinetic curve). It is significant to note that: a) the second-order kinetic model had R^2 values greater than the R^2 of the first-order

 Table 2. Textural and chemical characteristics and element analysis of activated carbon samples

parameters	Activated Carbon				
-	RSZ	RSP			
S _{N2} ^{a)} (m²/g)	771	613			
S _{ext} ^{b)} (m²/g)	91	126			
$V_2^{c}(cm^3/g)$	0.23	0.25			
V ₃ ^{d)} (cm ³ /g)	0.45	0.42			
V _{H20} ^{e)} (cm³/g)	0.41	0.41			
W _o (N ₂) ^{f)} (cm ³ /g)	0.29	0.21			
W _o (CO ₂) ^{g)} (cm ³ /g)	0.12	0.09			
$L_{o}(N_{2})^{h}(nm)$	1.57	1.66			
L _o (CO ₂) ⁱ⁾ (nm)	0.66	0.70			
W _o (N ₂) / W _o (CO ₂)	2.42	2.33			
Total acidic gro ups ^{j)} (µeq/g)	12.35	13.91			
Total basic groups ^{k)} (µeq/g)	6.33	0.00			
pH _{pzc} ^{I)}	5.80	2.70			
Oxygen ^{m)} (% wt)	43.29	55.91			
Ashes ⁿ⁾ (%)	39.68	48.26			
Si (%)	7.91	8.93			
Na (%)	0.06	-			
AI (%)	-	0.08			
Р (%)	2.22	37.19			
S (%)	0.36	0.10			
K (%)	0.27	0.19			
Ca (%)	2.38	0.32			
Cr (%)	1.11	1.64			
Mn (%)	0.14	0.10			
Fe (%)	6.83	5.77			
Со (%)	0.01	0.01			
Ni (%)	0.38	0.41			
Cu (%)	0.02	0.03			
Zn (%)	14.45	0.07			
Mo (%)	0.06	0.27			
CI (%)	0.32	-			
Ba (%)		0.05			

a) Surface area obtained from $N_{\rm 2}$ adsorption isotherms at 77 K.

b) External surface area obtained by mercury porosimetry.c) Pore's volume (diameter of 6.6–50 nm) obtained by mercury porosimetry.

 d) Pore's volume (diameter >50 nm) obtained by mercury porosimetry.

e) The volume of pores accessible to water determined by pycnometric densities.

f, g) Volumes of micropores obtained by N_2 and CO_2 adsorption, respectively.

h, i) Mean widths of micropores by $N_{\rm 2}$ and $CO_{\rm 2}$ adsorption, respectively, determined with the Dubinin equation.

j) The concentration of acidic groups determined by titration with NaOH (0.1 N).

k) The concentration of basic groups determined by titration with HCl (0.1 N).

I) pH of the point of zero charge.

m) Oxygen content by weight

n) Obtained at 900°C

model, b) $q_{pred,2}$ values were more similar to q_{exp} than $q_{pred,1}$ for all runs. These results show that the second-order model correlates to the experimental adsorption data much better than the first-order model.

Further, the adsorption kinetic constants were higher for carbon RSZ than those for RSP. This may be related to its higher volume of micropores and larger surface area than those for RSP. The adsorption rate of the activated carbons is relatively decreasing (MCPA > 2,4-D > DPA). Note the inverse proportion between absorption rate vs pollutant molecular size, MCPA of being smaller molecular size than DPA, see Table (1)

Adsorption isotherm.

Figure 1 represents the adsorption isotherm of DPA, 2,4-D and MCPA on carbons RSZ and RSP. Isotherm





 Table 3. Adsorption kinetic data after applying pseudo first and second order models to the selected pollutants on activated carbons RSZ and RSP

			Pesu	do 1 st orde	r	Pesudo 2 nd order			
Pollutant	Carbon	۹ _{exp} [mmol/g]	q _{pred,1} [mmol/g]	k₁ [1/h]	R ²	q _{pred,2} [mmol/g]	k₂ x10² [g/mmol/h]	R ²	
	RSZ	0.26	0.24	0.37	0.914	0.26	0.78	0.998	
DPA	RSP	0.24	0.23	0.16	0.851	0.25	0.34	0.997	
240	RSZ	0.34	0.32	0.46	0.881	0.34	2.31	0.976	
2,4-D	RSP	0.32	0.31	0.42	0.855	0.33	2.20	0.999	
МСРА	RSZ	0.39	0.32	1.77	0.939	0.35	10.68	0.999	
	RSP	0.39	0.31	1.43	0.931	0.34	7.26	0.996	

depicts the L form of Giles classification^{35, 36}, proposing that; a) the aromatic rings of all pollutant molecules were adsorbed in parallel to the surface of carbon, b) there is no major rivalry between pollutant molecules and water molecules for the active adsorption centers on the carbon.

Langmuir, Freundlich and Prausnitz-Radke adsorption isotherm model equations (9–11) are the most widely used models for this type of process:

$$X_{eq} = \frac{BX_m C_{Ae}}{1 + BC_{Ae}}$$
(9)

$$X_{eq} = K_F C_{Ae}^{1/nF}$$
(10)

$$q = \frac{aC_A}{1+bC_A{}^\beta} \tag{11}$$

These equations were used to evaluate the experiment results of the study to determine the type and mechanism of the adsorption processes. The adsorption isotherms model constants were evaluated by using a non-linear estimation method with *Statistica* software (release 7). The values of the isotherm constants as well as the average absolute percentage deviations are given in Table 4 by using the following equation:

$$\%D = \frac{1}{N} \sum_{i=1}^{N} \left| \frac{q_{exp} - q_{pred}}{q_{exp}} \right| \times 100\%$$
(12)

The comparison between Langmuir, Freundlich and Prausnitz-Radke models was presented at Table (4), Langmuir model fits the experiment data of DPA much better than other models with an average percentage deviations of less than 9.71% followed by Freundich (17.15%) and Prausnitz-Radke (19.67%). However, the Prausnitz-Radke model fits better to the experiment data of 2,4-D and MCPA than other models. Prausnitz--Radke model's average percentage deviation is less than 10.80% and 7.76% for 2,4-D and MCPA, respectively. This means that the adsorption of DPA into both activated carbons were monolayer and the adsorption of 2,4-D and MCPA is monolayer and multilayer hybrid. This explains the resulting order of adsorption rate of: a) MCPA the highest b) 2,4-D the second highest and c) DPA the lowest.

Taking a sample from Table 4, a relatively high maximum adsorption capacity (X_m): a) MCPA = 1.64, 2,4-D = 1.27, and DPA = 0.54 mmol/g on carbon RSZ b) MCPA = 1.64, 2,4-D = 1.23, and DPA = 0.61 mmol/g on carbon RSP. This shows that the adsorption capacity of carbon RSZ and carbon RSP for all pollutants, despite the surface area and volumes of micropores of both carbons, were approximately equal.

In previous works, Méndez-Díaz et al.³⁰ provided an extensive discussion on the adsorption mechanism of aromatic compounds on activated carbon. Establishing the dispersive interactions between π electrons of the graphene planes of the activated carbon surface. π electrons of the aromatic ring provide for this process. Note the ascending value of the adsorption capacity of both activated carbons – DPA < 2,4-D < MCPA. This is due to the use of two aromatic rings of DPA that effectively diminishes their electronic density. Note that the adsorbent–adsorbate interactions introduce resistance to the adsorption process.

The quantity of MCPA adsorbed was the highest. This is mainly due to MCPA having the smallest molecular size while DPA has the largest (Table 1). This makes these molecules to approach the smaller micropores size (L_o (CO₂)) (Table 2). Thus, the lower values of adsorbent-adsorbate relative affinity (BX_m) for DPA compared to MCPA.

Table 5 shows the occupied area augmentation order $S_{DPA} < S_{2,4-D} < S_{MCPA}$ for both activated carbons (RSZ and RSP). The maximum occupied area was of MCPA molecules: RSZ = 79.43%, RSP = 99.91%. These confirms that the adsorption of MCPA on both carbons was monolayer and multilayer. However, the occupied area was lower for 2,4-D and DPA: 61.51% and 32.48% for carbon RSZ; 74.93% and 46.15% for carbon RSP.

 Table 5. The occupied surface area by adsorbed molecules on the surface of activated carbons

Pollutant	Pollutant Carbon		S₀/S _{№2} ×100%
	RSZ	250.44	32.48
DFA	RSP	282.90	46.15
240	RSZ	474.25	61.51
2,4-0	RSP	459.31	74.93
МСРА	RSZ	612.42	79.43
	RSP	612.42	99.91

a) So: The occupied surface by adsorbed molecules

 Table 4. Parameters obtained by applying the Langmuir, Freundlich and Prausnitz-Radke equations adsorption isotherms of selected pollutants on carbons RSZ and RSP

				Langmu	ir		F	reundli	ich	Prausnitz-Radke			
Pollutant	С	X _m ^{a)} [mmol/g]	B ^{b)} [L/mmol]	BX _m ^{c)} [L/g]	X′ _m ×10 ⁻⁴ [mmol/m²/g]	%D	K _F ^{d)} [L/g]	1/n _F ^{e)}	%D	a ^{f)} [L/g]	b ^{g)} [L ^β /mmol ^β]	β^{h}	%D
	RSZ	0.54	23.35	12.61	7.00	9.71	0.58	0.22	9.73	6.59	0.01	1.21	19.67
DPA	RSP	0.61	25.23	15.39	9.95	4.12	0.68	0.25	17.15	9.20	0.02	1.22	13.35
240	RSZ	1.27	7.81	9.92	16.47	10.50	1.16	0.33	19.43	8.37	0.02	1.09	8.73
2,4-D	RSP	1.23	6.11	7.52	20.07	11.96	1.12	0.38	17.82	9.47	0.06	0.90	10.80
MCDA	RSZ	1.64	3.34	5.48	21.27	14.68	1.31	0.43	7.91	241888.00	8169.57	0.59	7.76
WCPA	RSP	1.64	3.86	6.33	26.75	11.38	1.31	0.40	5.21	453140.00	13037.50	0.61	5.15

a) X_m: Adsorption capacity

b) B: Langmuir constant

- c) $\mathsf{BX}_{\mathsf{m}}\!\!:\!\mathsf{Adsorbent}\!\!:\!\mathsf{adsorbate}$ relative affinity
- d) K_{F} : Relative adsorption capacity
- e) $1/n_{\text{F}}$: Sorption intensity or surface heterogeneity
- f) Prausnitz-Radke isotherm constant, L/g
- g) Prausnitz-Radke isotherm constant, $L^{\beta}/mmol^{\beta}$
- h) Prausnitz-Radke isotherm constant

These results further confirm that there are areas that molecules cannot access due to hindering effects.

Diffusion models

The external mass transport parameters must be determined first before correlating the adsorption kinetic data to the diffusional model. The molecular diffusion coefficient of pollutants in aqueous solution was assessed by using the equation 37 :

$$D_{AB} = \frac{7.4 \times 10^{-8} (\phi M_B)^{1/2} T}{\eta_b V_A^{0.6}}$$
(13)

Where: $\phi = 2.60$, $M_B = 18$ g/mol, $\eta_b = 0.89$ cp. Le Bas method [38] was used to estimate the VA values of DPA, 2,4-D and MCPA. These are provided in Table 1. The derived molecular diffusion coefficient is: a) DPA – 5.37×10^{-6} . b) 2,4-D - 7.46×10^{-6} and c) MCPA - 7.38×10^{-6} $cm^2/s.$

Furusawa and Smith³⁹, proposed the procedure to assess the experimental external mass transfer coefficient based on the following conditions; t \rightarrow 0, C_{Ar} \rightarrow 0 and C_A \rightarrow C_{A0}. If these conditions are introduced into equation (3), the equation below is derived:

$$\left[\frac{d\left(\frac{C_{A}}{C_{A0}}\right)}{dt}\right]_{t=0} = \frac{-mSk_{L,exp}}{V}$$
(14)

The term at the right of equation (14) is the rate of concentration decay at t = 0. This rate of decay was estimated using points t = 0 and t = 5 min of the concentration decay curve.

The experimental values of $k_{L,exp}$ obtained are listed in Table 6. The highest was observed in the case of MCPA followed by 2,4-D then by finally DPA. These confirm the results obtained from adsorption kinetics.

Pore volume diffusion model (PVDM) considers that that intraparticle diffusion is due to pore volume diffusion mechanisms. The relationship between the effective diffusion coefficient (D_{ep}) in a porous material and the molecular diffusivity (D_{AB}) can be described by various models. The simplest and commonly used model is based on the tortuosity factor, τ . In this model, D_{ep} can be estimated from the equation $^{40-42}$.

$$D_{ep} = \frac{D_{AB}\varepsilon_p}{\tau}$$
(15)

Leyva-Ramos and Geankoplis²⁸; Méndez-Díaz et al³⁰ and Leyva-Ramos et al.,43 studied intraparticle diffusion of organic compounds in activated carbons and recommended a tortuosity of $\tau = 3.5$ from a derived range of 1.57 to 6.57.

Numerical solution of the diffusion model

To start solving the diffusion equations (3) to (8), dimensionless variables are used to transform the diffusion model into a dimensionless model. Then a discretization step is performed to establish the finite difference approximation of the model. The dimensionless model is given as:

$$\frac{\mathrm{d}\phi_{\mathrm{A}}}{\mathrm{d}\theta} = -\frac{\mathrm{mSR}_{\mathrm{p}}^{2}k_{\mathrm{L,exp}}}{\mathrm{VD}_{0}} \left(\phi_{\mathrm{A}} - \eta_{\mathrm{A}}\big|_{\xi=1}\right)$$
(16)

$$\theta = 0, \quad \phi_A = 1 \tag{17}$$

$$\frac{\partial \eta_{\rm A}}{\partial \theta} = \frac{1}{(1 + \chi \omega) \left[\epsilon_{\rm p} + \omega \hat{F}(\eta_{\rm A}) \right]} \frac{1}{\xi^2} \frac{\partial}{\partial \xi} \left[\xi^2 \left(1 + \chi \omega \hat{F}(\eta_{\rm A}) \right) \frac{\partial \eta_{\rm Ar}}{\partial \xi} \right]$$
(18)

$$\eta_{A}=0, \quad \theta=0, \quad 0 \leq \xi \leq 1 \tag{19}$$

$$\left. \frac{\partial \eta_A}{\partial \theta} \right|_{\xi=0} = 0 \tag{20}$$

$$\frac{\partial \eta_{A}}{\partial \xi} \bigg|_{\xi=1} = \frac{(1+\chi\omega)R_{p}k_{L,exp}}{D_{0} \left[1+\chi\omega \hat{F}(\eta_{A})\big|_{\xi=1}\right]} \left(\phi_{A} - \eta_{A} \big|_{\xi=1} \right)$$
(21)

The radius of pores is discretized into N points with (N-1) distances. The mathematical model (16)-(21) consists of two coupled differential equation with mixed boundary conditions. The first equation is a first order ordinary differential equation in time variable while the other is a second order, parabolic, nonlinear partial differential equation. The coupled system relates the diffusion of concentration through the ambient solution to the diffusion through the pores and surfaces of nanoparticles. The numerical technique that has been used is finite difference with forward time forward space (FTFS) implementation where the normalized radius of the particle is divided linearly into N points with step $\Delta\xi$ and normalized time step $\Delta\theta$.

The first derivative at any point (i) with respect to dimensionless time, θ , is defined by $\frac{\partial \eta_A}{\partial \theta} = \frac{\eta_{A(i)}^{n+1} \cdot \eta_{A(i)}^n}{\Delta \theta}$ while the first and second derivatives with respect to dimensionless spatial variable at time (n) are given by $\frac{\partial \eta_{Ar}}{\partial \xi} = \left(\frac{{}^{-3\eta_{A(i)}^n + 4\eta_{A(i+1)}^n - \eta_{A(i+2)}^n}}{2\Delta \xi}\right), \frac{\partial^2 \eta_{Ar}}{\partial \xi^2} = \left(\frac{\eta_{A(i+1)}^n + \eta_{A(i+1)}^n - 2\eta_{A(i)}^n}{(\Delta \xi)^2}\right).$ Finally

the discretized model is given by

$$\frac{\phi_{A}^{n+1}-\phi_{A}^{n}}{\Delta\theta} = -\frac{mSR_{p}^{2}k_{L,exp}}{VD_{0}}\left(\phi_{A}^{n}-\eta_{A}^{n}\right|_{\xi=1}\right)$$
(22)

$$\frac{\eta_{A(i)}^{n+1} - \eta_{A(i)}^{n}}{\Delta \theta} = \frac{1}{(1 + \chi \omega) \left[\epsilon_{p} + \omega \hat{F}\left(\eta_{A(i)}^{n}\right)\right]} \begin{pmatrix} \frac{2}{\xi_{i}} \left(1 + \chi \omega \hat{F}\left(\eta_{A(i)}^{n}\right)\right) \left(\frac{-3\eta_{A(i)}^{n} + 4\eta_{A(i+1)}^{n} - \eta_{A(i+2)}^{n}}{2\Delta \xi}\right) \\ + \left(1 + \chi \omega \hat{F}\left(\eta_{A(i)}^{n}\right)\right) \left(\frac{\eta_{A(i+1)}^{n} + \eta_{A(i+1)}^{n} - 2\eta_{A(i)}^{n}}{(\Delta \xi)^{2}}\right) \\ + \left(\chi \omega \hat{F}\left(\eta_{A(i)}^{n}\right)\right) \left(\frac{-3\eta_{A(i)}^{n} + 4\eta_{A(i+1)}^{n} - \eta_{A(i+2)}^{n}}{2\Delta \xi}\right)^{2} \end{pmatrix}$$
(23)

Table 6. Calculation of mass transfer coefficient, diffusion coefficient, and tortuosity factor for investigated experiments

Pollutant	Carbon	С _{А0} [mg/L]	C _{Ae} [mg/L]	q₀ [mg/g]	k _{∟,exp} ×10 ³ [cm/s]	D _{ep} ×10 ⁷ [cm ² /s]	т
DPA	RSZ	96.02	16.80	79.23	0.72	4.31	2.27
	RSP	86.82	13.30	73.51	0.27	2.69	3.63
2,4-D	RSZ	104.40	15.36	89.04	0.79	4.52	3.00
	RSP	101.52	20.28	81.24	0.77	4.85	2.89
МСРА	RSZ	102.18	10.35	91.83	0.77	7.38	1.81
	RSP	102.18	9.82	92.36	1.09	2.21	6.04

with boundary and initial conditions:

 $\phi_{\Lambda}^{0} = 1, \ \eta_{\Lambda}^{0} = 0, \ -3\eta_{\Lambda}^{0} + 4\eta_{\Lambda}^{0} = 0$

$$\frac{-4\eta_{A(N-1)}^{n+1} + \eta_{A(N-2)}^{n} + 3\eta_{A(N)}^{n}}{\Delta\xi} = \frac{(1+\chi\omega)R_{p}k_{L,exp}}{D_{0}\left[1+\chi\omega f\left(\eta_{A(N)}^{n}\right)\right]} \left(\phi_{A}^{n} - \eta_{A(N)}^{n}\right)$$
(25)

(24)

To check the stability of the method, Von Neumann method is applied to check the stability. Replace $\eta_{A(i)}^{n+1}=\eta_{A(i)}^{n}e^{i\psi}, \eta_{A(i+1)}^{n}=\eta_{A(i)}^{n}e^{i\psi}, \eta_{A(i-1)}^{n}=\eta_{A(i)}^{n}e^{i\psi}, \eta_{A(i+2)}^{n}=\eta_{A(i)}^{n}e^{i2\psi}$ in equation (22) and (23). Equation (22) is transformed to $\phi_{A}^{n+1}=\phi_{A}^{n}-\frac{\Delta\theta \operatorname{mSR}_{P}^{2}k_{L,exp}}{VD_{0}}\left(\phi_{A}^{n}-\eta_{A}^{n}\right|_{\xi=1}\right)$. From which assuming neglected surface concentration one can get $G = \frac{\phi_{A}^{n+1}}{\phi_{A}^{n}} = 1 - \frac{\Delta\theta \operatorname{mSR}_{P}^{2}k_{L,exp}}{VD_{0}}$. To satisfy stability, then |G| < 1 which is satisfied. But for accurate calculations, we restricted the condition to be

$$\frac{\Delta \theta \left(m S R_{p}^{2} k_{L,exp} \right)}{V D_{0}} \leq \frac{1}{2}$$
(26)

So, the time step $(\Delta \theta)$ is chosen to satisfy the previous condition. By the same way, equation (23) is satisfied by the same condition.

Pore volume diffusion model (PVDM) by assuming $(D_{ep} \neq 0, D_s = 0)$

The PVDM model was used to interpret the derived experimental concentration decay curves. The mass transport parameters required to solve this model were D_{ep} and $k_{L,exp}$. D_{ep} was determined with equation (15) using $\tau = 3.5$ and $k_{L,exp}$ was calculated using equation (14). The optimal value of D_{ep} is obtained by taking the numerical solution of the PVDM model (\emptyset_{pred}) with the experimental concentration decay data then minimize the function:

$$Minimum = \sum_{1}^{N} (\phi_{exp} - \phi_{pred})^2$$
(27)

The optimum values of D_{ep} and the corresponding τ values were shown in Table 6. D_{ep} values were in the range of 2.21 x 10^{-7} to 4.85 x 10^{-7} cm²/s except for the case of MCPA on RSZ which was a little higher (7.38 x 10^{-7} cm²/s)

PVDM model with the derived optimal D_{ep} can predict points in the experimental data better than the same model using initial D_{ep} values at $\tau = 3.50$. It is safe to conclude that, for the studied systems, both methods are accurate in predicting data points in the experimental data. The tortuosity factor values in this study range from 1.81 to 6.04.

Surface diffusion model (SDM) by assuming $(D_{ep} = 0, D_s \neq 0)$

Surface diffusion model (SDM) considers that intraparticle diffusion is due to the surface diffusion mechanisms. It was calculated according to equation (8) by neglecting the part of pore volume diffusion.

Pore volume surface diffusion model (PVSDM) by assuming $(D_{ep} \neq 0, D_s \neq 0)$

Pore volume and surface diffusion model (PVSDM) considers that intraparticle diffusion is due to both pore volume and surface diffusion mechanisms. In order to solve the PVSDM model, $k_{L,exp}$ was calculated from equation (14) with an optimum D_{ep} derived from PVDM to minimize the error. Hence, the surface diffusion coefficient (D_s) was the remaining parameter to evaluate. To do this, a numerical solution of the PVSDM model (eq. 27) using concentration

decay data was derived then iterated for different values of D_s until it converges (minimum error). Figure 2 is a depiction of the experimental concentration decay data of MCPA onto RSZ and RSP. The figure shows that from the corresponding concentration decay curves of PVDM, SDM, and PVSDM, the best value of τ is obtained by PVDM. It is worth noticing that the PVDM and PVSDM models interpret the experimental data very satisfactorily.



Figure 2. Concentration decay curves for MCPA adsorption on activated carbons a) RSZ and b) RSP

The overall intraparticle diffusion of the different pollutants studied was evaluated. Specifically, the relative contribution of each diffusion mechanism in the said diffusion process. The following equations were used to estimate the mass transport due to pore volume diffusion (N_{AP}) and surface diffusion (N_{AS}) :

$$N_{AP} = -D_{ep} \frac{\partial C_{Ar}}{\partial r}$$
(28)

$$N_{AS} = -D_s \rho_p \frac{\partial q}{\partial r}$$
⁽²⁹⁾

The equation below was then used to estimate the relative contribution of pore volume diffusion to the overall intraparticle diffusion:

$$\frac{N_{AP}}{N_{AS}+N_{AP}} = \frac{D_{ep}\frac{\partial C_{Ar}}{\partial r}}{D_{s}\rho_{p}\frac{\partial q}{\partial r} + D_{ep}\frac{\partial C_{Ar}}{\partial r}}$$
(30)

The results are then plotted (Figure 3) using the following dimensionless radial positions; $\xi(r/R)$ (0/6, 1/6, 2/6, 3/6, 4/6, 5/6, and 6/6). Note that figure 3 is a plot just for MCPA on both activated carbons. The results revealed that the contribution of pore volume diffusion is over 85% for RSZ and 99% for RSP. These are percentages from the overall intraparticle diffusion as a function of the radial position and time. Note that from the rest of the systems studied; a) DPA on RSP that started at 42%, b) all else, the contribution of pore volume was more than 99%. Hence, pore volume diffusion is dominant in intraparticle diffusion of selected micropollutants during adsorption into activated carbon samples RSZ and RSP. In the succeeding sections, experimental adsorption data will be interpreted using PVDM model.



Figure 3. Contribution of pore volume diffusion to intraparticle diffusion at different radial position for MCPA adsorption on activated carbons a) RSZ and b) RSP

Effect of solution pH and Ionic Strength on adsorption process.

Influence of solution pH

One of the most important parameters in the adsorption process is the solution's pH. Figure 4a) and b) represent the influence of solution pH on the adsorption of 2,4-D, DPA and MCPA into carbons RSZ and RSP. The solution's pH evidently influence the adsorption process. The highest adsorption capacity for both carbons were at pH (4, 3, and 3) for DPA, 2,4-D and MCPA, respectively. Adsorption capacity is then diminished gradually by increasing the solution pH. It should be noted that aside from the solution pH, electrostatic interactions also play a significant role in the adsorption processes. Note that the solution pH is dominated by: i) pH_{pzc} of selected carbon (Table 2), and ii) the species distribution of pollutants as a function of solution pH (Table 1). Further, both carbons RSZ and RSP have positive charge density at solution $pH < pH_{pzc}$ and negative charge density at $pH > pH_{nzc}$. Deprotonation is performed on corresponding pollutant at DPA (pH) >4.66, 2,4-D (pH) >2.98 and MCPA (pH)> 3.14. These molecules, consequently, show a negative charge at pH higher than their pH_{PZC} .

Influence of ionic strength

The influence of ionic strength on the adsorption of DPA, 2,4-D and MCPA on carbons RSZ and RSP at



Figure 4. DPA, 2,4-D and MCPA adsorption capacity of activated carbon a) RSZ and b) RSP as a function of solution pH, T = 298 K and $C_0 = 500 \text{ mg/L}$

a solution pH around 3.20 (without addition of any reagents) is shown in Figs. 5a) and b), respectively. The ionic strength of the solution has minimal influence on the adsorption of all pollutants. Screening effect is mainly the cause of the miniscule reduction in MCPA adsorption observed in the solution containing NaCl⁴⁴ between the positive and trivial negative charge for RSZ and RSP, respectively. The DPA molecules were protonated at the working pH. Consequently, the presence of ions from NaCL supports adsorbent-adsorbate dispersion interactions due to a screening effect, by that





means improving the adsorption of DPA. Furthermore, a slight increase of the adsorption yield for 2,4-D in the presence of NaCL is attributed to the presence of NaCL in the solution. This caused a salting-out effect diminishing the solubility of 2,4-D, but improving its adsorption onto the carbon surface⁴⁵.

Adsorption process in dynamic regime

Adsorption of selected pollutants on columns of carbons RSZ and RSP were examined according to Rivera-Utrilla et al.³¹. Table 7 and Fig. 6 showed the result that the adsorbed quantity of pollutants at the breakthrough point $(X_{0.02})$ and the volume of water treated at the



Figure 6. Breakthrough curves for DPA, 2,4-D and MCPA adsorption on activated carbons a) RSZ and b) RSP, T = 298 K, pH = 3.20 and $C_0 = 200 \text{ mg/L}$

Table 7. Adsorption parameters obtained by the activated carbon columns

Pollutant	Carbons	X _{0.02} ^{a)} [mmol/g]	V _{0.02} ^{b)} [mL]	Φ ^{c)}	Φ ^{c)} H _{MTZ} ^{d)} R _{MTZ} x 10 ^{2 e)} [cm] [cm/min]		Du ¹⁾ [%]
DPA	RSZ	0.26	900	0.58	2.13	0.30	64.55
	RSP	0.10	336	0.57	1.52	0.95	75.71
2,4-D	RSZ	0.43	1140	0.71	1.26	0.53	71.90
	RSP	0.23	600	0.80	1.32	0.51	69.41
МСРА	RSZ	0.52	1320	0.60	1.16	0.26	80.59
	RSP	0.30	750	0.63	1.54	0.41	75.57

a) $X_{0.02}$: Amount of pollutant adsorbed at the breakthrough point of the column

b) $V_{0.02}$: Volume treated at the breakthrough point of the column

d) H_{MTZ}: Height of the mass transference zone

e) $R_{\mbox{\scriptsize MTZ}}\!\!:$ Rate of movement of the mass transfer zone

f) Du: Degree of utility

c) Φ: Fractional capacity of the mass transference zone

breakthrough point $(V_{0.02})$ for all pollutants was lower for carbon RSP than that for carbon RSZ. These coincide with the results from the static regime - higher adsorption capacity for carbon RSZ than for carbon RSP. Moreover, the amount of pollutants adsorbed in static regime was much higher than that obtained in dynamic regime which is a natural consequence of a shorter contact period between carbon and pollutant and high flow rate 30 . The mass transfer zone is extremely dependent on: a) the nature of the adsorbent-adsorbate interactions, b) carbon bed depth, c) inlet pollutant concentration and d) flow rate. The height of mass transfer zone was higher for carbon RSP bed than that for carbon RSZ bed for all pollutants except DPA. This confirmed that the carbon RSZ is more effective for the treatment of polluted water with 2,4-D and MCPA pollutants. Note, however, that DPA was adsorbed rapidly by RSP reflecting its degree of utility shown in Table 7. It is, therefore, safe to conclude that carbon RSZ should be used as column bed for the effective removal of 2,4-D and MCPA from aqueous solution while carbon RSP is more effective for the treatment of water with DPA pollutants.

CONCLUSION

Prepared activated carbons RSZ and RSP from rice straw showed high adsorption capacity for removal of DPA, 2,4-D and MCPA regardless of their chemical and textural characters.

The PVDM model fits satisfactorily to the experiment data of a single adsorption of selected pollutants on prepared activated carbons. The range of 1.81 to 6.04 tortuosity factor of the activated carbons was used. Out of the overall intraparticle diffusion, more than 99% is from pore volume diffusion. Except those cases of DPA on RSP and MCPA on RSZ - 42% and 85%, respectively. This confirms that the pore volume diffusion controlling mechanism of the overall rate and surface diffusion is negligible.

The adsorption capacity is significantly affected by the solution pH where the highest capacity of both carbons was observed in an acidic solution. On the contrary, the presence of NaCl in the solution did not have a significant effect on the activated carbon's adsorption capacity. The amount of pollutants removed by the activated carbons greatly decreased in dynamic regime. This is mainly due to the short contact period between carbon surface and pollutants. Activated carbon RSZ should be used as column bed for effective removal of 2,4-D and MCPA from aqueous solution while carbon RSP proved more effective for treatment of water polluted with DPA. The adsorption mechanism of DPA, 2,4-D, and MCPA onto carbons RSZ and RSP is controlled by dispersion interaction π - π electrons and electrostatic interaction. Moreover, the contribution of pore volume diffusion, from the overall rate of adsorption, is the controlling mechanism.

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ABBREVIATIONS

a – Prausnitz-Radke isotherm constant, L/g;

b – Prausnitz-Radke isotherm constant, $L^{\beta}/mmol^{\beta}$;

B – Constant related to adsorption energy;

C_A - The concentration of adsorbate in aqueous solution, mg/L;

 C_{A0} – Initial concentration of adsorbate in aqueous solution, mg/L;

CAr - The concentration of adsorbate within the particle at distance r, mg/L;

 $C_{Ar}|_{r=R}$ – The concentration of adsorbate at the external surface of the particle at $r = R_p$, mg/L;

 C_{Ae} – Concentration of adsorbate at equilibrium, mg/L; D_{AB} - Molecular diffusion coefficient at infinite dilution, cm^2/s :

 D_{ep} – Effective pore volume diffusion coefficient, cm²/s; D_s – The surface diffusion coefficient, cm²/s;

 k_1 – The rate constant of the first-order kinetic model, 1/h; k₂ – The rate constant of the second-order kinetic model, g/mg/h;

 $K_{\rm F}$ – Relative adsorption capacity;

k_{L, exp} - Experimental external mass transfer coefficient in liquid phase, cm/s;

m – Mass of adsorbent, g;

M_B – The molecular weight of water, g/mol;

N – Number of samples taken in the same experiment; N_{AP} - Mass transport due to pore volume diffusion, $mg/cm^2/s;$

 N_{AS} – Mass transport due to surface diffusion, mg/cm²/s; n_F - An indicator of sorption intensity or surface heterogeneity;

q – Mass of adsorbate adsorbed, mg/g or mmol/g;

q_{exp} - Experimental mass of adsorbate adsorbed, mg/g or mmol/g;

 $q_{pred,1}$ – Mass of adsorbate adsorbed predicted from the first-order kinetic model, mg/g;

q_{pred.2} - Mass of adsorbate adsorbed predicted from the second-order kinetic model, mg/g;

r – Distance in radial direction of the particle, cm;

 R_p – Radius of the particle, cm;

- S External surface area per mass of adsorbent, m^2/g ;
- T Temperature, K;
- t Time, min;
- V The volume of the solution, mL;

V_A – Liquid molar volume at the normal boiling point; X_{eq} - Quantity adsorbate adsorbed per unit mass of

adsorbent (mg/g);

X_m – Adsorption capacity (mg/g);

%D - Percentage of deviation;

 D_0 – Combined effective diffusivity;

F – Dimensionless ration.

Greek symbols

- B Prausnitz-Radke isotherm constant;
- $\varepsilon_{\rm p}$ Void fraction of particles;
- $\eta_{\rm b}$ The viscosity of water, cp;
- ϱ_p The density of adsorbent particles, g/mL;
- τ Tortuosity factor;
- ϕ Association parameter of water;

 ϕ_A – The dimensionless concentration of adsorbate in the solution;

 ϕ_{exp} – The experimental dimensionless concentration of adsorbate in the solution;

 ϕ_{pred} – The dimensionless concentration of adsorbate in the solution predicted with the diffusional models; ζ – Dimensionless distance;

 η_A – The dimensionless concentration of adsorbate within the particle at a distance r/R_p ;

 θ – Dimensionless time $D_0 t/R_p^2$;

 χ – Dimensionless diffusivities D_{es}/D_{en} ;

 ω – Dimensionless ratio $\rho_{\rm p}q_0/C_{\rm A0}$.

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