Efficiency of Pb(II) and Mo(VI) removal by kaolinite impregnated with zero-valent iron particles

Karolina Rybka¹, Katarzyna Suwała¹, Paulina Maziarz¹*, Jakub Matusik¹

¹ AGH University of Science and Technology, Faculty of Geology, Geophysics and Environmental Protection, Department of Mineralogy, Petrography and Geochemistry, al. Mickiewicza 30, Krakow, 30 059, Poland

* Corresponding author
e-mail: pmaziarz@agh.edu.pl

Received: April 13, 2017
Received in revised form: August 29, 2017
Accepted: August 29, 2017
Available online: September 30, 2017

Abstract. In this work, kaolinite modified with zero-valent iron was synthesized and used as a sorbent for Pb(II) and Mo(VI) removal from aqueous solutions. The obtained material was characterized by X-ray diffraction (XRD) and Fourier transform infrared (FTIR) spectroscopy. The methods revealed successful modification by the Fe⁰ particles precipitation on the surface of well-ordered kaolinite. The sorption experiment results showed a significant increase of sorption capacity in relation to the raw kaolinite. The kaolinite with 25% content of Fe⁰ was found to be the best material for Pb(II) and Mo(VI) removal, resulting in approximately 500 mmol·kg⁻¹ and 350 mmol·kg⁻¹ sorption, respectively. The possible mechanisms responsible for metals’ removal were identified as reduction by Fe⁰ ‘core’ and adsorption on the iron hydroxides ‘shell’. The study indicated that the obtained material is capable of efficient Pb(II) and Mo(VI) removal and may be an interesting alternative to other methods used for heavy metals’ removal.

Key-words: zero-valent iron particles, kaolinite, adsorption, Pb(II), Mo(VI)

1. Introduction

The increasing contamination of the environment with heavy metals has become a public health concern. This is because of their persistent nature and tendency to accumulate in living tissues. Therefore, there is a high demand for designing efficient methods of technological wastewater treatment.
Various treatment technologies have been reported for heavy metals’ removal, such as chemical precipitation (Meunier et al. 2006), oxidation-reduction (Ramos et al. 2009), adsorption (Rui et al. 2016), ion exchange (Oehmen et al. 2006) electrochemical treatment (Meunier et al. 2006), physical membranes (Zondervan, Roffel 2007), and filtration (Leupin, Hug 2005).

In practice, most of these methods turn out to be inefficient and damaging to the environment. Moreover, they have high energy requirements and may involve the use of harmful chemical reagents. Among the above methods, adsorption processes are one of the most commonly used because of their simplicity, relatively low cost, high effectiveness and wide range of possible applications in water treatment. Adsorption can be conducted with the use of many materials, both of organic and inorganic origin. Multiple methods of their modification are known, which have led to the improvement of their sorption properties. Many conventional and unconventional adsorbents have been used for heavy metals’ removal, including layered double hydroxides (LDH) (You et al. 2001; Hudcova et al. 2016), clay minerals (Suraj et al. 1998; Bhattacharyya, Gupta 2006; Zhang, Hou 2008; Üzüm et al. 2009), zeolites (Erdem et al. 2004; Szala et al. 2015), activated carbon (Patnukao et al. 2008; Xu et al. 2008), and graphene oxides (Ren et al. 2013; Liu et al. 2014).

Clay minerals are cost-effective, widely available and can be easily modified. Kaolinite is a 1:1 layered aluminum silicate clay composed of tetrahedral and octahedral sheets. The layers are linked together through hydrogen bonding between the oxygen atoms of the tetrahedral sheet and the OH groups of the octahedral sheet. Its chemical composition is Al₂Si₂O₅(OH)₄. To date, the kaolin group minerals have been reported as easily modified adsorbents for heavy metals’ removal (e.g. Suraj et al. 1998; Saada et al. 2003; Bhattacharyya, Gupta 2006, 2007; Unuabonah et al. 2008; Wang et al. 2015).

In recent years, research on zero-valent iron nanoparticles (nZVI) has been dynamically developed. Earlier experiments confirmed efficiency in heavy metals’ removal from water solutions, which is a result of nZVI’s high reactivity resulting from abundant reactive surface sites as well as the possibility of particle size control (Ponder et al. 2000; Üzüm et al. 2008; Li et al. 2016). Small particle size and powder state restrict nZVI application in real environmental conditions. The nZVI can also agglomerate and react with surrounding media, which results in poor mobility and subsequently in low removal efficiency. This is also connected with difficulties in nZVI migration into contaminated areas (Grieger et al. 2010). To minimize this effect, special composites, with the use of conventional adsorbents are prepared, which play the role of a support for nZVI (Shi et al. 2011; Kim et al. 2013; Wang et al. 2015).

The objective of this study was to obtain a kaolinite zero-valent iron composite capable of Pb(II) and Mo(VI) adsorption. Both elements can cause irreversible health effects for humans exposed to such a contaminated environment. Materials with different concentrations of zero-valent iron particles were prepared. The sorption experiments of Pb(II) and Mo(VI) were conducted to evaluate the adsorption efficiency, and the mechanisms responsible for Pb(II) and Mo(VI) removal.
2. Materials and methods

2.1. Materials

For the experiments, kaolinite sample collected from the Maria III kaolinite deposit (Lower Silesia Region, Poland) was used (K). Earlier studies revealed that the sample is mainly composed of kaolinite of high structural order and has a small admixture of illite and quartz (Koteja et al. 2015). The kaolinite was used as obtained, having a fraction <40 µm, without any purification. All used reagents were analytically graded. During the experiments, redistilled water was used.

2.2. Preparation of KFe⁰ composite

The synthesis of kaolinite composites followed a procedure reported earlier by Wang and Zhang (1997). The nZVI chemical synthesis can be described using the following reaction:

$$2\text{FeCl}_3 + 6\text{NaBH}_4 + 18\text{H}_2\text{O} \rightarrow 2\text{Fe}^0 + 6\text{NaCl} + 6\text{B(OH)}_3 + 21\text{H}_2$$  \hspace{1cm} (1)

In the experiment, the iron(III) chloride was used as an iron precursor and 1 M sodium borohydride as a reducing agent (Üzüm et al. 2009). In order to prevent iron oxidation, the synthesis was conducted in an argon atmosphere and at room temperature. The mass ratio of nZVI to kaolinite sample was set to 5, 10 and 25 wt%. The synthesis was performed in a round-bottom three-neck flask. Firstly, 150 ml of Fe(III) solution was prepared in ethanol. Then, 4.75 g of kaolinite was slowly added to the solution to obtain a homogenous suspension. In the next step, the sodium borohydride solution was prepared in 50 ml of redistilled water and added dropwise to the suspension of aqueous iron(III) chloride and kaolinite. The ethanol to water ratio was 3:1. The reductive agent was added in a 10% excess to ensure the complete reduction of Fe(III) to Fe⁰. The final products (KFe⁰₅, KFe⁰₁₀, and KFe⁰₂₅) were centrifuged (10 min, 4200 rpm), washed with ethanol and dried at 60ºC overnight.

<table>
<thead>
<tr>
<th>Sample</th>
<th>Fe⁰ amount [%]</th>
<th>Kaolinite [g]</th>
<th>FeCl₃·6H₂O [g]</th>
<th>NaBH₄ [g]</th>
<th>NaBH₄ (enlarged by 10%) [g]</th>
</tr>
</thead>
<tbody>
<tr>
<td>KFe⁰₅</td>
<td>5%</td>
<td>4.75</td>
<td>1.21</td>
<td>0.505</td>
<td>0.655</td>
</tr>
<tr>
<td>KFe⁰₁₀</td>
<td>10%</td>
<td>4.5</td>
<td>2.42</td>
<td>1.01</td>
<td>1.20</td>
</tr>
<tr>
<td>KFe⁰₂₅</td>
<td>25%</td>
<td>3.75</td>
<td>6.04</td>
<td>2.525</td>
<td>2.777</td>
</tr>
</tbody>
</table>

TABLE 1

List of reagents used during synthesis of the KFe⁰ samples, with amounts calculated from the stoichiometry of the reaction (1).
2.3. Characterization methods

The structural analysis of the mineral hybrids was done using X-ray diffraction (XRD) and Fourier transform infrared (FTIR) spectroscopy. The XRD patterns of powdered samples were recorded in the range of 2 – 73°2θ with 0.05°2θ steps, using a RIGAKU MiniFlex 600 diffractometer with CuKα (λ = 1.5418Å) radiation. The FTIR spectra of powdered samples were obtained with a Nicolet 6700 (Thermo Scientific). The IR spectra were recorded in transmission mode using KBr pellets (1mg sample per 200 mg KBr). For each measurement, 64 scans were collected in the range of 4000 – 400 cm⁻¹ and 4 cm⁻¹ resolution. The samples were also characterized by Scanning Electron Microscopy (SEM) – FEI Quanta 200 FEG with EDS detector. Samples were prepared by placing powdered material on a carbon tape. The X-ray Fluorescence (XRF) results were obtained by using a WD-XRF ZSX Primus II Rigaku spectrometer and SQX calculation software.

2.4. Adsorption isotherms

The adsorption studies were carried out for Pb(II) and Mo(VI) using initial concentrations in the range of 0.1 – 25.0 mmol·L⁻¹. The initial pH was adjusted to 5.0 using KOH and HNO₃ solutions. The Pb(II) and Mo(VI) stock solutions were prepared by dissolving Pb(NO₃)₂·4H₂O and Na₂MoO₄·2H₂O, respectively. The KFe₀ samples were added in the amount of 50 mg to 2.5 ml of metal solution (solid/liquid ratio of 20 g·L⁻¹). The suspensions were shaken for 24h at room temperature. Afterwards, the samples were centrifuged (5 min, 10000 rpm). The Pb(II) and Mo(VI) concentrations in equilibrium solutions were determined using the Atomic Absorption Spectroscopy (AAS) method: GBC SavanthAA spectrometer.

2.5. Adsorption kinetics

In the kinetic studies, a 1 mmol·L⁻¹ solution of Pb(II)/Mo(VI) was used. The initial pH was set to 5.0 ± 0.2. Then, 100 mg of each material sorbent was mixed with 5ml of the solution (20 g·L⁻¹ concentration) using a magnetic stirrer (100rpm) at room temperature. The suspension samples were collected after the reaction at 0.5, 1, 2, 4, 6, 8, 10, 15, 30 and 60min, and afterwards they were immediately filtered using a 0.22 μm PES membrane. The obtained kinetic data were evaluated by using pseudo-first-order (Eq. 2) and pseudo-second-order (Eq. 3) equations:

\[ \log(q_{eq}-q_t) = \log q_{eq} - (k_1t)/2.303 \]  \hspace{1cm} (2)
\[ t/q_t = 1/(k_2q_{eq}^2) + t/q_{eq} \]  \hspace{1cm} (3)

where \( q_{eq} \) and \( q_t \) are the sorption capacity at equilibrium and at time \( t \) (mmol·kg⁻¹), respectively; and \( k_1 \) (min⁻¹) and \( k_2 \) (kg·mmol⁻¹·min⁻¹) are the first order and second order rate constants, respectively.
3. Results and discussion

3.1. XRD results

The XRD analysis was conducted in order to investigate the mineralogical composition and the quality of the prepared materials (Fig. 1). The diffractogram of pure kaolinite showed the major basal spacing peak at approximately 7.18 Å. Moreover, a group of well-resolved peaks in the 19 – 24 2θ range was observed, indicating a high structural order of the mineral. After loading with zero-valent iron particles, the position of kaolinite basal reflection as well as the above-mentioned group of peaks did not change, confirming that the interlayer space was not altered. In turn, reflections at 2.92 Å and 2.03 Å were observed, attesting to the successful formation of Fe₀ particles exclusively on the kaolinite surface (Prabu, Parthiban 2013). It was noticed that the intensity of the reflections attributed to the Fe₀ formation increased with the increase of Fe₀ particles’ loading. At

![XRD patterns of kaolinite and Fe₀ composites](image)

Fig. 1. The XRD patterns of (a) pure kaolinite sample (K) and KFe₀ composites, (b) KFe₀5, (c) KFe₀10, and (d) KFe₀25.
higher Fe⁰ loading (25 wt%), an appearance of additional sharp reflection at approximately 2.82 Å was observed. Its presence can be connected with NaCl precipitation in the reaction of sodium (from the reducing agent NaBH₄) with chlorides (from FeCl₃·6H₂O). Also, a small peak at 2.79 Å could be observed, especially in a sample with the highest Fe⁰ loading. This is connected with the presence of siderite, precipitated in the iron reaction with adsorbed atmospheric CO₂.

### 3.2. FTIR results

The spectrum of pure kaolinite showed four distinct bands in the OH stretching region at 3620, 3652, 3668, and 3695 cm⁻¹. These bands confirmed the presence of well-ordered kaolinite, which is in agreement with the XRD patterns. The positions of these bands after Fe⁰ loading did not change. In turn, an intensity increase of the absorption band centered at approximately 3423 cm⁻¹ corresponding to the O–H vibration of the absorbed H₂O molecules was noticed. The intensity of this band increased systematically with the amount of loaded Fe⁰, indicating higher water adsorption affinity for the obtained kaolinite-based composites (Balan et al. 2001). In the range of 1000–400 cm⁻¹, the characteristic vibrations attributed to kaolinite aluminum silicate framework were noticed. Their positions and intensity were not affected by the Fe⁰ precipitation, indicating a lack of structural perturbations within the 1:1 layer.

![FTIR spectra](image)

Fig. 2. The FTIR spectra of (a) pure kaolinite sample (K) and KFe⁰ composites, (b) KFe⁰5, (c) KFe⁰10, and (d) KFe⁰25.
3.3. SEM/EDS results

Figure 3 shows the SEM images of the KFe\textsuperscript{0} samples. The brighter areas indicate regions having high electron density and are recognized as zero-valent iron (Fe\textsuperscript{0}). Figure 3a shows agglomerated kaolinite particles approximately 100 \(\mu\)m in size with Fe\textsuperscript{0} particles on the surface. The fibrous phase covering the kaolinite particles, which can be seen in Figure 3b–d, was recognized as iron oxyhydroxides. This confirmed that Fe\textsuperscript{0} underwent partial oxidation in the applied experimental conditions. Figure 3c and 3d show Fe\textsuperscript{0} particles, where the dimensions do not exceed 5 \(\mu\)m, although it should be noticed that the particle size was not unimodal. As reported earlier, the physical parameters of Fe\textsuperscript{0} particles such as size, dimension, and crystallinity can influence the rate of iron oxidation (Yan et al. 2012).

![Fig. 3. The SEM images of KFe\textsuperscript{0} samples.](image)

3.4. XRF results

Table 2 comprises the results of the XRF analysis of the K and KFe\textsuperscript{0} samples. An increasing amount of iron in the samples indirectly indicates an increasing amount of Fe\textsuperscript{0} in the composites, but to calculate the iron content for each sample the Fe content in K was subtracted. The Fe\textsuperscript{0} loading for the KFe\textsuperscript{0}5, KFe\textsuperscript{0}10, and KFe\textsuperscript{0}25 samples was calculated to
be 2.84%, 5.40%, and 12.06%, respectively. The results show that the evaluated values were nearly two times lower than the assumed ones. This may be due to insufficient reaction conditions, which favored the incomplete reduction of Fe(III) to Fe\(^0\). The presence of Na and Cl in the KFe\(^0\) samples is connected with substrates used for the synthesis.

TABLE 2

The XRF results for K and KFe\(^0\) samples.

<table>
<thead>
<tr>
<th></th>
<th>K</th>
<th>K - Fe(^0) 5%</th>
<th>K - Fe(^0) 10%</th>
<th>K - Fe(^0) 25%</th>
</tr>
</thead>
<tbody>
<tr>
<td>Mg</td>
<td>0.062714</td>
<td>0.088583</td>
<td>0.057588</td>
<td>0.051317</td>
</tr>
<tr>
<td>Al</td>
<td>10.37321</td>
<td>10.05265</td>
<td>9.256797</td>
<td>6.950239</td>
</tr>
<tr>
<td>Si</td>
<td>27.01694</td>
<td>23.12744</td>
<td>21.20204</td>
<td>16.07153</td>
</tr>
<tr>
<td>P</td>
<td>0.061971</td>
<td>0.034215</td>
<td>0.030222</td>
<td>0.023828</td>
</tr>
<tr>
<td>S</td>
<td>0.025669</td>
<td>0.032557</td>
<td>0.024267</td>
<td>0.02643</td>
</tr>
<tr>
<td>K</td>
<td>0.357376</td>
<td>0.300387</td>
<td>0.265894</td>
<td>0.216833</td>
</tr>
<tr>
<td>Ca</td>
<td>0.082189</td>
<td>0.055388</td>
<td>0.051743</td>
<td>0.032518</td>
</tr>
<tr>
<td>Ti</td>
<td>0.399156</td>
<td>0.339702</td>
<td>0.304941</td>
<td>0.230684</td>
</tr>
<tr>
<td>Cr</td>
<td>0.008108</td>
<td>0.006637</td>
<td>0.006295</td>
<td>0.002771</td>
</tr>
<tr>
<td>Fe</td>
<td>0.241649</td>
<td>3.084886</td>
<td>5.63874</td>
<td>12.3015</td>
</tr>
<tr>
<td>Sr</td>
<td>0.103162</td>
<td>0.081346</td>
<td>0.075934</td>
<td>0.057923</td>
</tr>
<tr>
<td>Zr</td>
<td>0.011253</td>
<td>0.068479</td>
<td>0.055375</td>
<td>0.048935</td>
</tr>
<tr>
<td>Pb</td>
<td>0.05867</td>
<td>0.046137</td>
<td>0.044373</td>
<td>0.036111</td>
</tr>
<tr>
<td>Na</td>
<td>-</td>
<td>0.534987</td>
<td>0.615329</td>
<td>0.628312</td>
</tr>
<tr>
<td>Cl</td>
<td>-</td>
<td>0.2277</td>
<td>0.1064</td>
<td>1.0743</td>
</tr>
</tbody>
</table>

3.5. Adsorption experiment results

As shown in Figure 4a, the removal of Pb(II) varied with the amount of zero-valent iron particles. The sorption increased with increasing concentration of the Fe\(^0\). For the highest Pb(II) initial concentrations, a slight decrease of adsorption was observed. The highest sorption capacity estimated from the isotherm plateau was observed for the KFe\(^0\)25 sample and was equal to ~500 mmol·kg\(^{-1}\). The observed values were much higher than observed for the pure Maria III kaolinite, which was equal to ~10 mmol·kg\(^{-1}\) (Koteja, Matusik 2015). This proved that kaolinite coated with zero-valent iron particles had a significantly higher adsorption affinity toward Pb(II) than the raw kaolinite. After 24 h of the adsorption experiment, the pH increased significantly. It reached values close to 9.0 for the KFe\(^0\)5 and KFe\(^0\)10, and 6.0 for the KFe\(^0\)25 (Fig. 4a). Along with the increase of sorption, the pH decreased. Only for the KFe\(^0\)25 sample did the pH drop below the initial pH, which was set to 5.0.
All the used materials showed a removal percentage close to 100% for the Pb(II) concentrations up to 2 mmol·L⁻¹ (Fig. 4b). As the Pb(II) initial concentration increased, the Pb(II) uptake decrease was observed. This decrease was more pronounced in the case of sorption onto KFe₀.₅ and KFe₀.₁₀ where the final removal was equal to 14% and 26%, respectively, for the initial concentration of 25 mmol·L⁻¹. Whereas for the KFe₀.₂₅, the removal efficiency decreased to 43% for the highest Pb(II) concentration.

The adsorption of anions by kaolinite including Mo(VI) ionic species is possible only to a small extent, due to the lack of its anion-exchange properties (Zachara et al. 1988). The coating of kaolinite with zero-valent iron particles significantly improved the sorption capacity of Mo(VI). In analogy to Pb(II), the sorption increased with the amount of loaded Fe⁰. The maximal values measured at the highest initial concentrations were in the range of 175 – 220 mmol·L⁻¹ for the KFe₀.₅ and KFe₀.₁₀. The highest adsorption capacity, equal to 350 mmol·kg⁻¹, was observed for the KFe₀.₂₅. These values were much higher than those observed for pure and modified kaolinites with other anions, including As(V), P(V), S(VI), and N(V) (Matysik 2014). Previous sorption studies indicated that sorption capacity was equal to 5 mmol·kg⁻¹ for the initial Mo(VI) concentration of 5 mmol·L⁻¹ (Rybka 2017).

In all cases, the final pH was higher than the starting value of 5.0. The pH increase was the highest for the lower Mo(VI) concentrations and equal to ~9.0. In turn, the increase was less significant for higher concentrations where the final value was in the 5 – 7 range. The pH range after the sorption experiment varied between 5.5 and 9.0. The final pH can result from iron oxidation and the production of hydroxyl ions (Crane, Scott 2012), and can be influenced by the metal concentration in the solution.

As shown in Figure 5B, the removal percentage for KFe₀.₂₅ was equal to 80% for the lowest Mo(VI) concentration. Along with the Mo(VI) concentration increase, the percentage uptake decreased to approximately 35-50%. The KFe₀.₅ seemed to have the highest percentage removal, whereas the KFe₀.₅ and KFe₀.₁₀ showed similar results for Mo(VI) concentrations in the range of 1–25 mmol·L⁻¹.
3.6. Adsorption kinetics

For the Pb(II) sorption experiment, after only 30 sec all Pb(II) was adsorbed by each material (KFe⁰⁵, KFe⁰¹⁰, and KFe⁰₂⁵). The results of the Mo(VI) sorption kinetic experiment are shown in Figure 6. The Mo(VI) sorption proceeded with a lower rate and kinetics depending on the material. For the KFe⁰⁵, the maximum uptake of 65% was reached after 60 min, but after 15 min the sorption efficiency was equal to 55%. For the KFe⁰¹⁰ and KFe⁰₂⁵ materials, 100% sorption efficiency of Mo(VI) occurred after 8 min and 5 min, respectively. As shown in Table 3, the kinetic data for the Mo(VI) fit much better to a pseudo-second-order equation in the case of the KFe⁰¹⁰ and KFe⁰₂⁵ materials. However, for the KFe⁰⁵ agreement both with the pseudo-first-order and pseudo-second-order equations was observed.

<table>
<thead>
<tr>
<th>Sample</th>
<th>Pseudo-first-order R²</th>
<th>k₂</th>
<th>Pseudo-second-order qₑₒₚ</th>
<th>R²</th>
</tr>
</thead>
<tbody>
<tr>
<td>KFe⁰⁵</td>
<td>0.9715</td>
<td>0.0131</td>
<td>18.48</td>
<td>0.994</td>
</tr>
<tr>
<td>KFe⁰¹⁰</td>
<td>0.3928</td>
<td>0.0089</td>
<td>28.90</td>
<td>0.9836</td>
</tr>
<tr>
<td>KFe⁰₂⁵</td>
<td>0.2168</td>
<td>0.0200</td>
<td>34.48</td>
<td>0.9941</td>
</tr>
</tbody>
</table>
3.7. Adsorption mechanisms

To investigate the adsorption mechanisms, the XRD analysis was conducted on the KFe\textsuperscript{025} samples after the Pb(II) and Mo(VI) sorption experiments. As shown in Figure 7, the samples after reaction with Pb(II) and Mo(VI) do not show characteristic peaks attributed to Fe\textsuperscript{0}, in contrast to the raw KFe\textsuperscript{025}. The mechanism responsible for such phenomena is iron oxidation (Crane, Scott 2012). However, no characteristic peaks for iron oxides or iron hydroxides were found. This could be due to their amorphous or poor crystalline character, which was favored by fast precipitation, as well as the content of the oxidation products that can be below the XRD detection limit.

Zero-valent iron is susceptible to corrosion when exposed to the presence of oxygen (Eq. 4;5) – in aqueous media or air.

\[
\begin{align*}
2\text{Fe}\textsuperscript{0}(s) + 4\text{H}^+(aq) + \text{O}_2(aq) & \rightarrow 2\text{Fe}^{2+} + 2\text{H}_2\text{O}(l) \quad (4) \\
2\text{Fe}^{0}(s) + 2\text{H}_2\text{O}(l) & \rightarrow 2\text{Fe}^{2+} + \text{H}_2(g) + 2\text{OH}^-(aq) \quad (5)
\end{align*}
\]

The kinetics of this process is very rapid and takes place even in controlled conditions. The corrosion product is Fe(II), which can turn into Fe(III) (Eq. 6;7) after further oxidation process.

\[
\begin{align*}
2\text{Fe}^{2+}(s) + 2\text{H}^+(aq) + \frac{1}{2}\text{O}_2(aq) & \rightarrow 2\text{Fe}^{3+} + \text{H}_2\text{O}(l) \quad (6) \\
2\text{Fe}^{2+}(s) + 2\text{H}_2\text{O}(l) & \rightarrow 2\text{Fe}^{3+} + \text{H}_2(g) + 2\text{OH}^-(aq) \quad (7)
\end{align*}
\]
In such reactions, protons are consumed with the simultaneous production of hydroxyl ions, which increases the pH. The Fe(II) and Fe(III) ions in aqueous solution can form precipitates, such as iron oxides and hydroxides. The iron in zero-valent form can be responsible for the reduction or sorption of contaminants because of its core-shell structure (Fe\(^0\) ‘core’ and iron-oxide ‘shell’) created on a porous surface (Crane, Scott 2012). It was earlier reported that an oxidized shell covering the Fe\(^0\) particles starts to form at pH above 4.5 (Scott et al. 2011). Thus, as the initial pH in sorption experiments was set to 5.0, the presence of such iron particles exhibiting dual chemical character is highly possible.

As shown, the Pb(II) sorption increased with the loading amount of Fe\(^0\). An increasing amount of Fe\(^0\) in a sample increases the number of active sites on the material surface (Zhang 2013). The kaolinite supporting material prevented the aggregation of iron nanoparticles, providing more specific surface area for Pb(II) sorption (Zhang et al. 2010).
The Pb removal from aqueous solutions is not only a result of adsorption processes, but also a reduction in which Pb(II) is reduced simultaneously by the KFe⁰, while precipitation may also be involved (Arancibia-Miranda et al. 2014). The possible mechanism responsible for Pb(II) removal can be given by the following reaction (Ponder et al. 2000):

$$2\text{Fe}^0 + 3\text{Pb}^{2+} + 4\text{H}_2\text{O} \rightarrow 3\text{Pb}^0 + 2\text{FeOOH} + 2\text{H}^+$$

(8)

The initial pH of the metal solutions was adjusted to 5.0 before adding the KFe⁰, and increased to approximately 9.0 during the reaction, mainly as a result of oxidation of the Fe⁰ by water (Kim et al. 2013). The high value of pH caused either negative charging of the KFe⁰ surface or Pb(OH)₂ precipitation in the solution and on the surface of KFe⁰ (Zhang et al. 2010).

A large increase of pH after sorption experiments at low Mo(VI) concentrations can be connected with the transformation of Fe⁰ into Fe(II) and Fe(III), subsequently resulting in the formation of an iron hydroxide ‘shell’ (Li et al. 2016). The Mo(VI) removal in such conditions may be due to both reduction by Fe⁰ and adsorption by iron hydroxide, but the reduction process seems to be dominant and can be described by the following reaction (Scott et al. 2011):

$$\text{MoO}_4^{2-} + 4\text{H}^+ + 2e^- \rightarrow \text{MoO}_2 + 2\text{H}_2\text{O}$$

(9)

4. Conclusions

This work showed a successful kaolinite modification with zero-valent iron particles, which is suitable for Pb(II) and Mo(VI) removal from aqueous solutions. The material synthesis resulted in Fe⁰ precipitation on the kaolinite surface, simultaneously with the presence of iron hydroxides, representing a ‘core-shell’ structure responsible for the material’s sorption properties. The loading of Fe⁰ on kaolinite was confirmed by XRD and XRF analysis, while SEM analysis was conducted to show the Fe⁰ surface distribution.

The obtained material showed a significant increase of sorption capacity in relation to the raw kaolinite. The measurements showed that the increasing content of Fe⁰ increased the sorption of Pb(II) and Mo(VI). The application of the material with 25% content of Fe⁰ resulted in the highest sorption equal to approximately 500 mmol·kg⁻¹ for Pb(II) and 350 mmol·kg⁻¹ for Mo(VI).

The Pb(II) kinetic experiment showed that all Pb(II) was removed after only 30 sec. The highest sorption rate in the case of Mo(VI) was observed for the KFe⁰25 material. This confirmed the controlling role of Fe⁰ on the kinetics. A decrease of the Fe⁰ amount led to a lower sorption rate.

The sorption mechanisms were determined as a reduction induced by highly reactive Fe⁰ particles and adsorption on iron hydroxides. This was supported by pH measurements and solid-state analyses of the materials after adsorption processes. The observations were in agreement with earlier reports.

The overall results indicate that the application of Fe⁰-modified kaolinite can effectively remove Pb(II) and Mo(VI) from aqueous solutions, and thus can be an efficient and environmentally friendly substitute in water treatment technologies.
Acknowledgements. This project was supported by the National Science Centre, Poland, under a research project awarded by Decision No. 2016/21/N/ST10/00390.

5. References


Matusik, J. (2014). Arsenate, orthophosphate, sulfate, and nitrate sorption equilibria and kinetics for halloysite and kaolinites with an induced positive charge. *Chemical Engineering Journal*, 246, 244-253. DOI: 10.1016/j.cej.2014.03.004.


Ryłka, K. (2017). Efektywność oczyszczania roztworów wodnych z wybranych anionów przez nanokompozyty otrzymane na bazie kaolinitu ze złoża Maria III, (Efficiency of selected anions removal from aqueous solutions by nanocomposites derived from Maria III kaolinite.), MSc thesis, AGH University of Science and Technology, Krakow, Poland. [in Polish].


