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THE EFFECT OF SQUEEZE PIN DIMENSION AND OPERATIONAL PARAMETERS ON MATERIAL HOMOGENITY OF ALUMINIUM HIGH PRESSURE DIE CAST PARTS

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Abstract

The present paper is an experimental study on the squeeze pin effect on the high pressure die cast aluminium parts, as a way of improvement of material homogenity on various and big wall thickness castings. Squeeze is used in high pressure die casting technology for optimizing homogenity of big wall thicknesses of die cast parts working as structural, mechanical and hydraulic components, made of different aluminium alloys such AlSi alloys. The objective of this research is to highlight the primary and secondary effects of squeezing on the structural homogenity of high pressure die cast aluminium parts, as well as the dependence of the effects on the squeeze pin dimensions and the operating parameters.

Key words: high pressure die casting, AlSi alloy, squeeze pin, shrinkage, cold flow, porosity

1. Introduction

High pressure die-casting process is one of the most common manufacturing processes of high complexity and precise parts. The challenge of the process in most cases is the homogenity of the castings material, which is influenced by several controllable parameters, such as speeds, pressures, temperatures, and changeover points between phases [1-8].

Our previous published results identified causes that affect the homogenity of certain aluminium high pressure die cast parts and leaded to the improvement of die casting process of automotive gearbox suspension brackets [9-10].

Present research work focuses on the material homogenity improvement by reduction of porosity, internal cold flow and shrinkage porosity, using squeeze pin technology. The scope of the squeeze pin is, by applying it in a massive area (big alloy volume), to modify the structure and density of the part during solidification stage. The homogenity levels were analyzed from the perspective of current standards [11-14]. ASTM E505 - Reference radiographs for inspection of aluminium and magnesium die castings

[13] was used as reference standard for the results interpretation.

2. Materials and methods

The experiments were designed for the suspension bracket area of a part produced from AlSi9Cu3(Fe) with high pressure die casting technology, which concentrates a big volume of alloy due to functional design reasons.

This massive bracket area of the part with normal hole precast high pressure die cast process presents shrinkage porosity problems as well as internal cold flows, fact well known and predicted from solidification simulation phase with Flow3D software, as indicated in the Figure 1.

The tests were planned with a mold equipped with squeeze pin and related guiding bush, as well as hydraulic cylinder connected to the high pressure die cast machine, an Italpresse 1650 Tn machine with possibility to control and monitor the squeeze time in and out through its shot control system and program connected to PC [15-23]. Analyze of samples was performed on an MU2000 Yxlon X-ray machine.

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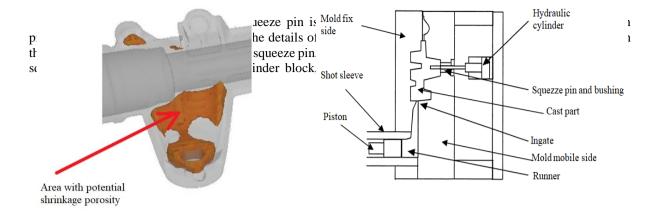


Fig. 1: Solidification simulation with Flow 3D software

Fig. 2: Schematic solution of the mold with squeeze pin

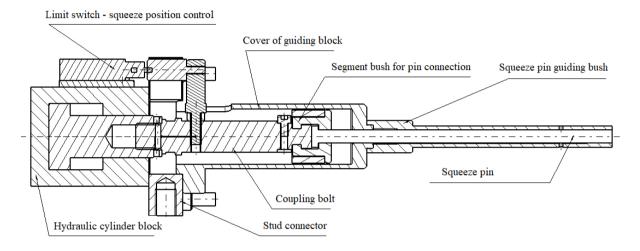


Fig. 3: Details of the squeeze design

Several dimensions – diameters and active lengths - of the squeeze pin, as well as different squeeze times,

summarized in the Table 1, have been planned for the experimental test.

Test number	Test code	Squeeze pin diameter [mm]	Squeeze depth [mm]	Squeeze time [s]
	10_15_0		15	0
	10_15_0.5	10		0.5
1	10_15_1			1
1	10_15_1.5			1.5
	10_15_2			2
	10_15_2.5			2.5
	10_7.5_0			0
	10_7.5_0.5	10	7.5	0.5
2	10_7.5_1			1
2	10_7.5_1.5			1.5
	10_7.5_2			2
	10_7.5_2.5			2.5
	9_15_0	9	15	0
3	9_15_0.5			0.5
	9_15_1			1
	9_15_1.5	9	13	1.5
	9_15_2			2
	9_15_2.5			2.5

4	9_7.5_0 9_7.5_0.5 9_7.5_1 9_7.5_1.5 9_7.5_2 9_7.5_2.5	9	7.5	0 0.5 1 1.5 2 2.5
5	8_15_0 8_15_0.5 8_15_1 8_15_1.5 8_15_2 8_15_2.5	8	15	0 0.5 1 1.5 2 2.5
6	8_7.5_0 8_7.5_0.5 8_7.5_1.5 8_7.5_1.5 8_7.5_2 8_7.5_2.5	8	7.5	0 0.5 1 1.5 2 2.5

3. Results and discussion

Each test has been performed according to the test plan. 10 samples have been produced in serial conditions for each test code with the corresponding parameters, by maintaining at the same level the values of the other process parameters, and varying only the parameters of the squeeze pin: diameter, depth and time. The samples have been analyzed on an X-ray machine adjusted to a voltage of 115 kV and intensity of 10 mA. Radioscopy pictures have been captured at scale 2:1.

The representative radioscopy pictures captures of Test 3 - diameter of squeeze pin 9 mm, depth 15 mm and squeeze times 0 s, 0.5 s, 1 s, 1.5 s, 2 s, and 2.5 s are summarized in Figure 4.

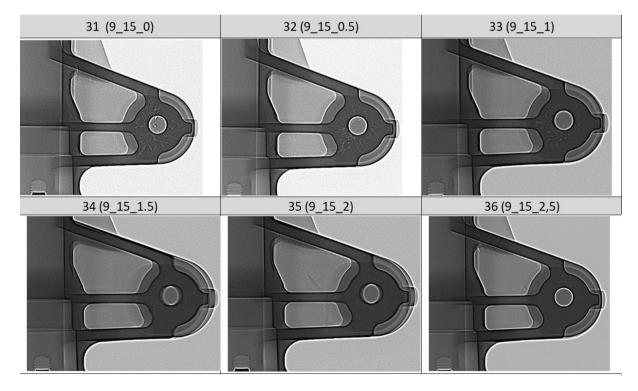


Fig. 4: Representative radioscopy pictures captures of Test 3

The representative radioscopy pictures captures of Test 4 - diameter of squeeze pin 9 mm, depth 7.5 mm and squeeze times 0 s, 0.5 s, 1 s, 1.5 s, 2 s, and 2.5 s

are summarized in Figure 5. For each test 60 samples have been produced; totally for tests 1, 2, 3, 4, 5 and 6, 360 samples have been produced.

In case of all the tests for all samples the tendency of shrinkage presence and its dependency on squeeze time parameter can be observed. The appearance of a dark line can be observed at 1.5 - 2 seconds squeeze time delay in most of the cases with squeeze depth 15 mm. Table 2 presents the summary of all test results.

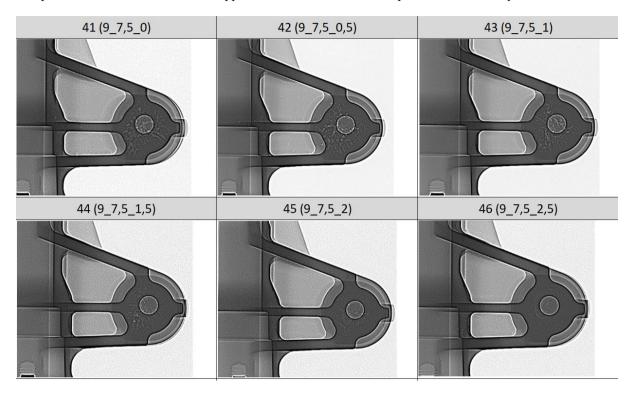


Fig. 5: Representative radioscopy pictures captures of Test 4

Table 2: Summary of all tests results

Test number	Test code	Squeeze pin diameter [mm]	Squeeze depth [mm]	Squeeze time [s]	Shrinkage level Target ASTM E505 Level 1	Dark line presence	
1	10_15_0	10	15	0	NOK	no line	
	10_15_0.5			0.5	NOK	no line	
	10_15_1			1	NOK	no line	
1	10_15_1.5	10		1.5	OK	Line present	
	10_15_2			2	OK	Line present	
	10_15_2.5			2.5	OK	Line present	
	10_7.5_0	10	7.5	0	NOK	no line	
2	10_7.5_0.5			0.5	NOK	no line	
	10_7.5_1			1	NOK	no line	
	10_7.5_1.5			1.5	NOK	no line	
	10_7.5_2			2	Limit OK	Line present	
	10_7.5_2.5			2.5	OK	Line present	
	9_15_0	9	15	0	NOK	no line	
	9_15_0.5			0.5	NOK	no line	
2	9_15_1			1	NOK	no line	
3	9_15_1.5			1.5	OK	Line present	
	9_15_2			2	OK	Line present	
	9_15_2.5			2.5	OK	Line present	
	9_7.5_0	9	7.5	0	NOK	no line	
4	9_7.5_0.5			0.5	NOK	no line	
	9_7.5_1			1	NOK	no line	
	9_7.5_1.5			1.5	NOK	no line	
	9_7.5_2		1		2	NOK	no line
	9_7.5_2.5			2.5	NOK	no line	

5	8_15_0	8	15	0	NOK	no line
	8_15_0.5			0.5	NOK	no line
	8_15_1			1	NOK	no line
	8_15_1.5			1.5	Some OK	Line present
	8_15_2			2	Some OK	Line present
	8_15_2.5			2.5	Limit OK	Line present
6	8_7.5_0	8	7.5	0	NOK	No line
	8_7.5_0.5			0.5	NOK	No line
	8_7.5_1			1	NOK	No line
	8_7.5_1.5			1.5	NOK	No line
	8_7.5_2			2	NOK	No line
	8_7.5_2.5			2.5	NOK	No line

Scope of pin diameter and depth is to compensate volume. In this respect and also based on the results of the tests is evident that the shrinkage level became better and achieves the standard requirement at short squeeze delay time of 1.5 seconds. It is the case of test 1.4. with pin diameter 10 mm, squeeze depth 15 mm and squeeze time delay 1.5 seconds.

With smaller pin diameter and reduced squeeze depth the standard requirement was not achieved. It is the case of test 6.6. with pin diameter 8 mm, squeeze depth 7.5 mm and squeeze time delay of 2.5 seconds.

In case of the same pin diameter and depth we can observe the tendency and dependency of improvement of material homogenity with the increase of the squeeze time delay: as longer is the delay the better is the homogenity. This dependency is reflected in the captures from Figure 4 and 5.

As a secondary effect the appearance of a dark line can be observed. Its dependence is also direct with the bigger volume compensation and delay of the squeeze time: as longer is the delay the bigger is the size of the dark line. This dark line looks compact, but different as the rest of the area nearby. It might be a macro segregation of the alloying elements as a secondary effect of the resulted pressures and temperatures. Current standards don't evaluate the category level of this phenomenon.

The study of this phenomenon will be the subject of a future research work as well as its influence on the casting mechanical properties. Other future research directions would be:

- assessment of the alloy density in the squeezed area;
- determination of the hardness in the squeezed area:
- characterization of the chemical composition of the dark line area.

4. Conclusions

The use of squeeze pins is a practical method of material homogenity improvement for parts with high risk of shrinkage porosity resulted also from flow and solidification simulations for the high material volume areas.

The additional pressure coming from the squeeze pins have as a direct effect higher density of material and appearance of dark lines. This is normal and direct effect of the additional pressure applied during solidification phase.

The tests performed show the "indirect" relation between the dark lines and porosity. When dark lines do not appear, squeeze pin effect is smaller and porosity level is increased. When squeeze pin effect is better, dark lines appear naturally but only in this situation porosity level requested can be achieved.

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