Development and validation of a UPLC-MS method for determination of atazanavir sulfate by the “analytical quality by design” approach

CHANDNI SAHA^{1*}
 N. VISHAL GUPTA¹
 R. S. CHANDAN²

¹ Department of Pharmaceutics
 JSS College of Pharmacy
 JSS Academy of Higher Education &
 Research, Mysuru, Karnataka 570015
 India

² Department of Pharmaceutical
 Chemistry, JSS College of Pharmacy
 JSS Academy of Higher Education &
 Research, Mysuru, Karnataka 570015
 India

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A UPLC-MS method for the estimation of atazanavir sulfate was developed using the “analytical quality by design” approach. The critical chromatographic quality attributes identified were retention time, theoretical plates and peak tailing. The critical method parameters established were percent of organic modifier, flow rate and injection volume. Optimization performed using Box-Behnken Design (BBD) established 10 % organic modifier, 0.4 mL min⁻¹ flow rate and 6-μL injection volume as the optimum method conditions. Atazanavir sulfate eluted at 5.19 min without any interference. Method validation followed international guidelines. The method has proven linearity in the range of 10–90 μg mL⁻¹. Recovery was between 100.2–101.0 % and precision within the accepted limits (RSD 0.2–0.7 %). LOD and LOQ were 2.68 and 8.14 μg mL⁻¹, resp. Stress testing stability studies showed atazanavir sulfate to degrade under acidic and basic conditions. The suggested technique is simple, rapid and sustainable. It is, therefore, suggested for routine analysis of atazanavir sulfate.

Keywords: atazanavir sulfate, UPLC-MS, “analytical quality by design”

Atazanavir sulfate is the first protease inhibitor with a simplified dosing profile (1). Protease inhibitors are among the most potent classes of antiretroviral drugs; however, due to their pill burden and side effects, the prescribing choice has shifted to non-nucleoside reverse transcriptase inhibitors. Recent developments in the fixed-dose combination and highly active antiretroviral therapy has made atazanavir sulfate a promising drug (2, 3). Atazanavir sulfate is chemically known as 3,12-bis(1,1-dimethylethyl)-8-hydroxy-4,11-dioxo-9-(phenylmethyl)-6-[[4-(2-pyridinyl)phenyl]methyl]-2,5,6,10,13-pentaazatetradecane-dioic acid dimethyl ester. It has a favorable resistance profile that provides it with the advantage of being a first-line therapy drug (3). Having a large potential, the drug has been explored by determining its genotoxic impurities (4), determination in dried blood spot (5),

* Correspondence, e-mail: chandnisaha7@gmail.com

some bioanalytical methods (6, 7), development of stability indicating methods (8, 9), assay method (10) and pharmacokinetic studies (11–13). However, method development through the “analytical quality by design” (AQbD) approach has not been addressed.

Overcoming the challenges of one factor at a time (OFAT), the QbD approach has amended the pharmaceutical quality management system (14). QbD systematically builds quality within the process, eliminating quality testing at the end of the process (15). QbD approach commences by defining the quality targets and identifying the critical quality attributes. The paradigm advances by identifying the critical process and material parameters through sound risk assessment studies (16), further through the concept of experimental designs/design of experiments (DOE); as a result, the multifactor effects on selected responses are observed. DOE also reduces the number of experiments to be performed when a large number of factors (inputs) are involved (14). The concept of QbD has been present in various industries since the 1970s but was introduced into the pharmaceutical industry in 2004 through Pharmaceutical cGMPs for the 21st Century initiative (17); it is also reflected in ICH Q8-Q10 guidelines (18–20). The QbD approach has been adopted as “analytical quality by design” (AQbD) for analytical method development with peripheral alterations in terminologies (21).

The focus of this paper is therefore to maneuver the paramount advantages of QbD to analytical method development using ultra performance liquid chromatography-mass spectrometry (UPLC-MS). Method development through the AQbD approach for the determination of atazanavir sulfate constitutes the novelty of this paper. Unlike the existing methods for determination of atazanavir sulfate, the current method avoids the use of complex buffer systems; thus, the use of a simple mobile phase adds to the novelty of the paper.

EXPERIMENTAL

Chemicals and samples

The gift sample of atazanavir sulfate, active pharmaceutical ingredient, was received from Laurus Labs, India. Atazanavir sulfate capsules, Atazor 300 mg, from Emcure Pharmaceuticals Ltd., India, were obtained from the local market. Thermo Fisher Scientific, USA, furnished LCMS grade acetonitrile. GR grade ammonium acetate was from Merck, Germany. HPLC type I water was from the Millipore Direct-Q® 3 UV water purification system, Merck Millipore, Germany.

Chromatographic conditions and apparatus

Acquity UPLC® (Waters, USA) using a reverse-phase Acquity UPLC BEH C18 (1.7 μm , 1 mm x 50 mm) column coupled in-line with a Synapt G2 (Waters, USA) mass spectrometer aided by a high resolution quantitative time-of-flight (QuanTof™) analyzer and featuring an ultra-fast electron multiplier, hybrid analog-to-digital (ADC) detector, was used for all chromatographic separations. Electrospray ionization interface in positive mode directed column eluent to the mass spectrometer. The mass spectrometer operated in sensitivity mode using capillary voltage of 1.8 kV and cone voltage of 17 V. The desolvation gas flow rate was 300 L h⁻¹, while the source and desolvation gas temperature were 100 and 200 °C,

resp. The gradient mode mobile phase was composed of 10 mmol L⁻¹ ammonium acetate as solvent A and acetonitrile as solvent B. Organic modifier percent, mobile phase flow rate and injection volume were varied according to the experimental runs from DOE.

Preparation of standard stock solution

Standard stock solution of 1.0 mg mL⁻¹ was obtained by dissolving accurately weighed atazanavir sulfate in water. Serial dilutions of the standard stock solution gave working standards between 10 and 100 µg mL⁻¹. Working standards were filtered using 0.2-µm Phenex PTFE syringe filters (Phenomenex, USA) before being injected.

Method development using the AQbD approach

The first step in the AQbD approach is to define the objectives of the method, collectively termed as analytical target profile (ATP)/quality target method profile (QTMP) (22–24). The ATP of the current method was to develop a simple, accurate, precise, robust and specific method meeting the critical quality attributes (CQAs). CQAs are the most vital parameters that, within their defined limits, ensure the quality of the method (29). The CQAs identified for the suggested UPLC-MS method development were retention time, theoretical plates and peak tailing. The acceptance criterion for theoretical plates was > 2000 and < 2 for peak tailing (26, 27). Further, risk factors identification through initial trials, risk analysis through Ishikawa/fish bone diagram and evaluation by failure mode and effect analysis (FMEA) were used to uncover the high risk factors as critical method parameters (CMPs).

Initial screening of factors through fraction factorial design (FFD). – Initial screening of factors/method parameters aids to discover the CMPs that significantly cause variations in CQAs and eliminates factors which are just noise. Fraction factorial design (FFD), resolution IV with one generator (2⁴⁻¹) from Design Expert® v.11.0 software produced eight experimental runs for the initial screening of four factors at two levels. The factors at their low and high levels were organic modifier: 10 and 30 %, flow rate: 2 and 6 mL min⁻¹, injection volume: 0.2 and 0.6 µL and column temperature: 25 and 45 °C. Using Pareto charts and model significance values, the significant factors were resolved.

Optimization of selected factors using the Box-Behnken design (BBD). – The significant factors, organic modifier (at 10 and 30 %), flow rate (2 and 6 mL min⁻¹) and injection volume (0.2 and 0.6 µL), were optimized at their low and high levels using BBD; they produced 17 experimental runs. These experiments were performed using 50 µg mL⁻¹ working standard solution of atazanavir sulfate. The results were analyzed by goodness of fit (*R*²), *p*-values, adjusted *R*² and predicted *R*², and the lack-of-fit values by Design Expert® v.11.0 software. Variations in CQA were comprehended through contour plots and 3D graphs. Numerical optimization was used to optimize and select the method conditions best fitting the CQAs with desirability near one. Criteria for optimization of retention time and peak tailing were selected to be “in range” of their minimum to maximum values obtained during the experiments, while the criterium was set to the maximum value for theoretical plates. Graphical optimization with 99 % tolerance assisted exploring the design space within the set criteria.

Analytical method validation

Following ICH Q2(R1) guidelines (28), parameters like linearity, accuracy, precision, limit of detection (LOD), limit of quantification (LOQ) and selectivity were assessed during the method validation. AQbD approach provides the advantage of establishing the design space, a region within which any changes to factor (CMP) values do not significantly affect the method development, thus, incorporating robustness into the process and, therefore, testing of robustness at the end of method development can be omitted (18).

Linearity. – Working standard solutions prepared in the range of 10–100 $\mu\text{g mL}^{-1}$ were filtered through a 0.2-micron syringe filter and injected into the chromatograph, each in 3 replicates. Total ion chromatograms (TIC) were obtained and the calibration curve was plotted to establish the linear relationship by the least squares method.

Accuracy. – Accuracy was tested using the standard addition method. The capsule formulation sample was spiked with a known amount of the active pharmaceutical ingredient at 80 % (40 $\mu\text{g mL}^{-1}$), 100 % (50 $\mu\text{g mL}^{-1}$) and 120 % (60 $\mu\text{g mL}^{-1}$). The resultant solution was analyzed in six replicates. Percentage recoveries were calculated and reported (Table III).

Precision. – The intra-day and intermediate (inter-day) precision were calculated from the peak areas of 40, 50 and 60 $\mu\text{g mL}^{-1}$ working standard solutions of atazanavir sulfate, injected on the same day and on two consecutive days, resp. ($n = 6$). Similarly, precision of the formulation analysis using 40, 50 and 60 $\mu\text{g mL}^{-1}$ solutions of Atazor was measured.

LOD and LOQ. – LOD and LOQ were calculated using calibration curve data, following the formula $\text{LOD} = 3.3 \times \text{SD}/\text{slope}$ and $\text{LOQ} = 10 \times \text{SD}/\text{slope}$, where SD is the standard deviation of the regression line (29, 30).

Selectivity. – Selectivity of the method was demonstrated by injecting the blank, working standard solution and sample (commercial formulation) solution and monitoring the elution of analyte.

Stability testing (stress conditions)

Pursuant to ICH Q1A (R1) and ICH Q1 B guidelines (31, 32), stress testing of the drug substance can help identify the likely degradation products, which can in turn help establish the degradation pathways and the intrinsic stability of the molecule and validate the stability indicating power of the analytical procedure used.

Acid, base and thermal (moist heat) degradation. – Ten mg of atazanavir sulfate was dissolved in 10 mL 0.1 mol L⁻¹ HCl, 0.1 mol L⁻¹ NaOH and water, resp., in a round bottom flask and refluxed at 80 °C for 60 min. Samples were collected at 60 min and cooled to room temperature (28 °C). The acid and base degraded samples were then neutralized with 0.1 mol L⁻¹ NaOH and 0.1 mol L⁻¹ HCl, resp. All samples were further diluted with water to 50 $\mu\text{g mL}^{-1}$, sonicated for 5 min, filtered and injected into the UPLC-MS system.

Oxidative degradation. – Ten mg of atazanavir sulfate reacted with 10 mL of 3 % and 30 % H₂O₂ separately in two round bottom flasks at room temperature (28 °C) for 60 min.

Samples collected after 60 min were cooled to room temperature (28 °C), diluted with water to 50 µg mL⁻¹, sonicated for 5 min, filtered and injected into the UPLC-MS system.

Photolytic degradation. – Ten mg of atazanavir sulfate in a clean quartz tube was placed under UV light (320 nm) for 1 day. The drug was sampled thereafter, dissolved in water to a concentration of 1.0 mg mL⁻¹ and further to 50 µg mL⁻¹. This solution was sonicated for 5 min, filtered and injected into UPLC-MS.

RESULTS AND DISCUSSION

Risk assessment studies

In order to develop a method within the acceptable range of CQAs, it is essential to have a thorough understanding of the method parameters and their effects. A risk assessment study methodically identifies the factors/parameters that can have a substantial effect on the CQAs. ICH Q9 lists 9 risk management tools (19), of which the Ishikawa/fishbone diagram and failure mode and effect analysis (FMEA) are extensively used in the QbD approach (33). The Ishikawa diagram/fishbone diagram dissects the method development process into various fractions such as men, material, method, *etc.*, and each fraction provides an insight into factors/parameters that can affect the CQAs. Further, FMEA aids to rank and prioritize these factors into low, medium, and high risks based on a composite score called the risk priority number (RPN). The RPN is calculated based on the impact of risk on the method, frequency of occurrence and the ability to detect the failure (impact * occurrence * detectability) (14).

In the present method, initial trials, Ishikawa diagram/fishbone diagram (Fig. 1) and FMEA tools, resp., identified, analyzed and prioritized the risk factors associated with the method development process. Using the knowledge from initial trials, identified risks were evaluated for their impact, occurrence, and detection, to calculate the RPN. Factors that

Fig. 1. Ishikawa diagram/fishbone diagram for estimating the parameters affecting CQAs.

Table I. Identifying high risk factors through the risk priority number (RPN)

Factor/process	Failure affect (s)	Severity (impact)	Occurrence	Detection	RPN
Solubility	Recovery, peak area, theoretical plates	3	1	4	12
Sonication	Separation quality	1	1	4	4
Ionization	Peak detection	4	1	1	4
Organic modifier	Retention time, separation quality	4	1	4	16
Organic modifier portion	Retention time, separation quality, peak area	5	5	4	100
Injection volume	Peak area, separation quality, peak area	5	5	4	100
Separation mode	Retention time, separation quality, peak area	3	1	4	12
Flow type	Retention time	3	1	4	12
Flow rate	Retention time, separation quality, peak area	5	5	4	100
Column temperature	Separation quality	4	5	4	80
Column type	Retention time, separation quality, peak area	4	1	4	16

RPN – risk priority number: < 43 (low risk factors), 44–83 (medium risk), > 84 (high risk).

Table II. Optimization through the Box-Behnken design: factor conditions and results

Standard run	Run order	Factor				CQAs	
		Organic modifier (%)	Flow rate (mL min ⁻¹)	Injection volume (μL)	Retention time (min)	Theoretical plates ^a	Peak tailing
15	1	20	0.4	4	4.92	6556	0.82
16	2	20	0.4	4	4.91	6488.7	0.81
12	3	20	0.6	6	4.37	7861.3	0.70
10	4	20	0.6	2	4.37	6892	0.74
6	5	30	0.4	2	4.29	6331	0.69
13	6	20	0.4	4	4.7	6808.5	0.79
1	7	10	0.2	4	7.22	6409.51	1.01
5	8	10	0.4	2	5.2	7642.93	0.761
7	9	10	0.4	6	5.21	9028	0.78
4	10	30	0.6	4	3.6	6764	0.63
3	11	10	0.6	4	4.71	6034.72	0.61
11	12	20	0.2	6	6.4	6688.4	1.03
8	13	30	0.4	6	4.29	7380.47	0.64
9	14	20	0.2	2	6.37	5438.1	1.09
14	15	20	0.4	4	4.92	6556	0.78
17	16	20	0.4	4	4.92	6556	0.81
2	17	30	0.2	4	5.86	3982.8	0.82

CQAs – critical quality attributes

^a Per column length.

Fig. 2. Pareto chart representing the significance of risk factors on chosen CQAs: a) retention time, b) theoretical plates and c) peak tailing.

could have high severity (impact), high occurrence (probability) and low detectability were assigned the value of 5 on a scale of 1–5 while factors showing low severity, low occurrence and high detectability scored near 1. The RPN values classified the organic modifier percent, flow rate, and injection volume as highrisk factors while column temperature was a mediumrisk factor (listed in Table I). Further, these factors were screened using DOE.

Initial screening of factors through fraction factorial design (FFD). – The four factors screened through FFD (2^{4-1}) showed a parallel relation between the main effects. Proving the lack of interactions, their evaluation followed the first-order polynomial equation given as follows:

Retention time (min)

● Design points above predicted value

○ Design points below predicted value

3.6 7.22

X1 = A: Organic modifier (%)

X2 = B: Flow rate (mL min⁻¹)

Actual factor

C: Injection volume = 6 μ L

Theoretical plates

● Design points above predicted value

○ Design points below predicted value

3982.8 9028

Peak tailing

● Design points above predicted value

○ Design points below predicted value

0.61 1.09

Fig. 3. 3D surface plots for responses: a) retention time, b) theoretical plates and c) peak tailing.

$$Y = \beta_0 + \beta_1 X_1 + \beta_2 X_2 + \beta_3 X_3 + \beta_4 X_4$$

where β_0 is the intercept and β_1 – β_4 are coefficients of each factor, X being the factor value and Y is the response. The results were analyzed using a Pareto chart as shown in Fig. 2. It shows that the flow rate and organic modifier had a significant effect on retention time and theoretical plates, while the flow rate and injection volume influenced peak tailing. High R^2 values for retention time (0.9895), theoretical plates (0.9945) and peak tailing (0.9556) inferred that these factors caused significant variations in the CQAs; hence, optimization was carried out using these three factors. Column temperature did not influence the CQAs significantly and thus it was set to an intermediate value of 35 °C during optimization experiments. Screening of factors prior optimization helps reduce the experimental burden and errors.

Optimization and design space. – The results presented in Table II revealed quadratic relations between the CMPs and the CQAs; thus, evaluation followed the second-order polynomial equation:

$$Y = \beta_0 + \beta_1 X_1 + \beta_2 X_2 + \beta_3 X_3 + \beta_4 X_1 X_2 + \beta_5 X_2 X_3 + \beta_6 X_1 X_3 + \beta_7 X_1^2 + \beta_8 X_2^2 + \beta_9 X_3^2$$

where β_0 is the intercept and β_1 – β_9 are coefficients of each term, X being the factor value and Y is the response.

The results (Table II) were analyzed by analysis of variance (ANOVA) and fit statistics by observing their p -values and goodness of fit (R^2), resp. The R^2 values for retention time (0.9883), theoretical plate (0.9848) and peak tailing (0.9904), all being close to one and the p -values observed to be < 0.05 , justified the significant influence of CMPs on the variation in CQAs ($p < 0.05$ rejects the null hypothesis and accepts the alternative hypothesis that factors are significant). The difference between the adjusted R^2 and predicted R^2 found to be less than 0.2 indicated the absences of inflated factor inclusion in the model. Adjusted R^2 values decrease if insignificant factors are included in the model, causing an increased difference between adjusted and predicted R^2 values, which is an indication of a model with unnecessary factors. The lack of fit being not significant proved that the model was safe to explore the design space/method operable design region (MODR).

Influence of CMPs on retention time, theoretical plates and peak tailing was in curvilinear fashion as observed through the contour plots and 3D surface plots (Fig. 3). The 3D surface plots in Fig. 3a show long retention time towards lower organic modifier percent and short retention time towards higher organic modifier percent at increased flow rate. Theoretical plates were high in case of lower organic modifier percent, flow rate around 0.4 mL min⁻¹ and higher injection volume, as shown in Fig. 3b; Fig. 3c shows lowered peak tailing at low and high organic modifier percent at a flow rate of > 0.4 mL min⁻¹.

Numerical optimization was used to figure out the method conditions with desirability near one. The criteria during optimization were set to be “in range” of minimum to maximum values of the retention time and peak tailing obtained from 17 experiments, while maximum for theoretical plate. From the 2D contours plots in Fig. 4, we can interpret the area with high desirability (orange), low (blue) to high (orange) retention time, high (orange) theoretical plates and low (blue) peak tailing. Cumulatively from the results of 3D surface plot, numerical optimization and contour plots, the optimized method conditions

All responses

● Design Points

0.000 1.000

X1 = A: Organic modifier (%)

X2 = B: Flow rate (mL min⁻¹)

Actual factor

C: Injection volume = 6 μ L

Fig. 4. 2D contour plots for desirability, retention time, theoretical plates/column length and peak tailing.

Overlay Plot

Retention time (min)

TI Low

TI High

Theoretical plates

TI Low

Peak tailing

TI Low

TI High

● Design Points

X1 = A: Organic modifier (%)

X2 = B: Flow rate (mL min⁻¹)

Actual Factor

C: Injection volume = 6 μ L

Fig. 5. Overlay plot showing the method operable design region.

Table III. Accuracy and precision studies

Formulation sample (atazanavir, $\mu\text{g mL}^{-1}$) ^b	RSD (%)	Spiked concentration ($\mu\text{g mL}^{-1}$)	Total concentration found ($\mu\text{g mL}^{-1}$) ^b	RSD (%)	Recovery (%)		
50.5 (50.0 ^a)	0.5	40.0	90.8	0.2	100.4		
		50.0	100.8	0.2	100.2		
		60.0	111.2	0.3	100.5		
Concentration found ($\mu\text{g mL}^{-1}$) ^b		RSD (%)					
Intra-day		Inter-day		Intra-day		Inter-day	
40.0 ^a	40.2	40.3	0.3	0.5			
50.0 ^a	50.3	50.3	0.7	0.7			
60.0 ^a	60.2	60.3	0.3	0.4			
Atazanavir sulfate ($\mu\text{g mL}^{-1}$)	Concentration found ($\mu\text{g mL}^{-1}$) ^b			RSD (%)		Model recovery (%)	
Intra-day		Inter-day		Intra-day	Inter-day	Intra-day	Inter-day
40.0	40.4	40.3	0.5	0.7	101.0	100.8	
50.0	50.3	50.1	0.6	0.6	100.6	100.2	
60.0	60.4	60.2	0.5	0.7	100.7	100.3	

^a Atazor capsules; concentration upon label claim.

^b Mean value, $n = 6$.

established were 10 % organic modifier, 0.4 mL min⁻¹ flow rate and 6- μL injection volume. Mobile phase was run in the following gradient percentage of acetonitrile, organic modifier: initial 10 %, 4–5 min 50 %, 7–8 min 10 %. Graphical optimization was used to explore

Table IV. Comparison of the new method with the existing ones

Mobile phase	Retention time (min)	Ref.
Phosphate buffer (pH 6)-acetonitrile (43:57, V/V)	16.20	34
Solvent A: KH_2PO_4 buffer (0.02 mol L ⁻¹ , pH 3.5), solvent B: acetonitrile	12.5	35
Mobile phase A: 0.01 mol L ⁻¹ KH_2PO_4 (pH 3.6), mobile phase B: acetonitrile	9.18	36
MeOH-H ₂ O (9:1, V/V) pH 3.55 (with HAc)	8.32	8
55 % acetonitrile, 45 % water, 0.15 % HAc, 4 mmol L ⁻¹ NH_4Ac	8.30	37
0.02 mol L ⁻¹ $\text{NH}_4\text{H}_2\text{PO}_4$ buffer-acetonitrile-MeOH (30:25:45, V/V), pH 2.5 (with H_3PO_4)	3.00	9
Solvent A: 10 mmol L ⁻¹ NH_4Ac , solvent B: acetonitrile	5.19	This paper

the design space/MODR. Design space (yellow area) indicated the region where changes to the optimized conditions will be tolerated and will be within the operable quality (Fig. 5), thus, confirming the robustness of the method for the intended use.

Fig. 6. a) TIC of atazanavir sulfate eluted at 5.19 min, b) mass spectrum of the eluted peak.

Fig. 7. TIC of: a) mobile phase (blank), b) standard atazanavir sulfate, c) commercial capsule of atazanavir sulfate and d-f) their respective mass spectra.

Fig. 8. a) BPI chromatogram of acidic degradation of atazanavir sulfate, b) mass spectra of eluted peaks from acidic degradation of atazanavir sulfate, c) BPI chromatogram of basic degradation of atazanavir sulfate, d) mass spectra of eluted peaks from basic degradation of atazanavir sulfate, e–h) BPI chromatograms of thermal, photolytic, 3 % H₂O₂ oxidative and 30 % H₂O₂ oxidative degradation of atazanavir sulfate, resp.

Under optimized conditions, atazanavir sulfate was eluted at 5.19 min; the 705 *m/z* value from the mass spectrum confirmed the presence of atazanavir sulfate without any interference. Fig. 6a shows the total ion chromatogram (TIC) and Fig. 6b the mass spectrum of the eluted peak.

Method validation

The developed analytical method was linear in the range of 10–90 $\mu\text{g mL}^{-1}$. The calibration plot statistically proved the linearity ($y = 56.18x + 0.3573$; $R^2 = 0.9999$) indicating good linear fit. The method was reported to be accurate with recovery between 100.2 – 101.0 % and precise with RSD ranging from 0.2–0.7 % (Table III). Calculated LOD and LOQ of atazanavir sulfate were 2.68 and 8.14 $\mu\text{g mL}^{-1}$, resp. The method was shown to be selective with the analyte being identified as a sharp peak at 5.19 min both in standard and sample solutions without any interference from the blank (Fig. 7). The optimized and validated method proved to be better than several existing liquid chromatographic methods in terms of retention time and simple mobile phase composition (see Table IV).

Further, the systematic approach to optimized method conditions and statistical justification make the entire process distinct from the regular practice.

The proposed method was applied to the assay of a commercial capsule formulation. The mean % assay was 101.0 % of the declared amount with RSD of 0.5 % ($n = 6$).

Stability testing (stress testing)

Stress testing studies showed atazanavir sulfate to degrade under acidic and basic conditions while being stable under thermal, oxidative and photolytic experimental conditions. Fig. 8 shows the results of degradation through base peak intensity (BPI), for it is much clearer to view all degradation peaks unlike in TIC.

CONCLUSIONS

Unlike the existing approaches for method development, the AQbD approach to method development made the entire process rational, systematic and embedded robustness within the method. The proposed method achieved the ATP by systematically identifying the risk factors and optimizing them to perceive the method conditions best fitting the defined CQAs. The method gave a detailed insight into the benefits of screening factors before optimization, thus reducing significant factors to organic modifier percent, flow rate and injection volume. Optimization using experimental design founded the method conditions, which was justified by statistical analysis. Following the established design space during method development can control experimental errors. Statistical significance of the method conditions along with satisfactory alignment to validation guidelines made the method sustainable and reflected its reliability. This approach shows that methodical planning and orderly execution can reduce the risk, experimental burden and errors, and thus its application to various research areas is foreseen.

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Supplementary material available upon request.

Acronyms, abbreviations, symbols. – Ac – acetate, ADC – analog-to-digital, AQbD – analytical quality by design, ATP – analytical target profile, BPI – base peak intensity, BBD – Box-Behnken design, BEH – ethylene bridged hybrid, CMPs – critical method parameters, CQAs – critical quality attributes, DOE – design of experiments, FMEA – failure mode and effects analysis, FFD – fraction factorial design, MeOH – methanol, MODR – method operable design region, OFAT – one factor at a time, PTFE – polytetrafluoroethylene, QbD – quality by design, QTMP – quality target method profile, RPN – risk priority number, TIC – total ion chromatograms

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