

HEATING CONTROL OF HEATED TWIN RADIOSONDE HUMIDITY SENSOR BASED ON DMC

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ABSTRACT

In order to effectively solve condensation and icing problems of radiosonde in low-temperature environment at high altitude, humidity sensor heated automatic alternately to remove pollution and improve the measurement accuracy. Heat experiments obtained the curve of rising temperature and responsible time on heated twin humidity sensor in normal temperature and pressure, by expanded responsible curve to obtain heated model of twin heated humidity sensor and by the analysis of heating model, use DMC and PID control for heating respectively. Simulation results show that the DMC control meets the practical requirements of measure at high altitude.

Keywords: DMC; twin heated humidity sensor; expanded responsible curve; Heating Control

INTRODUCTION

Altitude humidity with height has greater spatial resolution, sounding humidity sensor should have a high sensitivity, response speed, small size and other characteristics [1]. The humidity sensor is susceptible to clouds, rain and other humid hypothermia environments. Especially, when encountering with cold water, it prone to be frozen, thus, the measurement of humidity is likely influenced. Conventional approach is to heat the radiosonde humidity sensor to eliminate environmental impacts during the process of rising [2].

PID control method is widely used in process control because of its simple and reliable principle, as well as advantages like astatic property and cheap price. Meanwhile, it is a relatively mature classic controller [6-8]. However, this

system is based on a non-linear model (saturated, latency, backlash, etc.), and its uncertainty makes it difficult to achieve an expected result under certain conditions. Moreover, traditional PID control algorithm is difficult to predict the effect of control. Disadvantages like low control accuracy and poor robustness also exists [9-11]. Fuzzy control is flexible and adaptable because it does not require accurate mathematical model of the object. However, regardless the types of pure fuzzy controller, every controller is essentially a non-linear PD control that actually does not play an integral role in controlling. Sometimes the control process is not smooth, and the steady-state error is also hard to be reduced to a desired level [12-16].

Dynamic Matrix Control (DMC) is a predictive control algorithm based on the step response of the object, which is suitable for asymptotic stability of linear objects, in a rolling optimization and online error correction to ensure the control of accuracy and the parameter, environmental change of robustness. The whole algorithm includes a predictive model, rolling optimization and feedback correction [12-14]. It is directly based on the model of the step response of the object, thus can avoid parameter identification in the usual transfer function or state space equation model. DMC is a kind of optimal control technology because this control algorithm can effectively solve problems of delay process by using multi-step predictive value technology. Meanwhile, according to the predictive value of output with a given value of minimum deviation of the quadratic performance index is implemented to control. It has the advantages of simple algorithm, small computational amount and strong robustness, which can be applied to the stability of linear systems. In addition, the dynamic characteristics of the system with pure lag or non-minimum phase are not affected by the direct application of the algorithm [17-21]. For resolving issues related to rain (cloud) drops soaked, freezing and other conditions that causing the humidity sensor to detect inaccurate moisture signals, a dual heating radiosonde humidity sensor was proposed in this paper based on the traditional heating control method, which effectively reduces the impact of humidity measurement accompanied with external environment [22-29].

THE OUTLINE OF HEATING PRINCIPLE

System's humidity sensor uses humicap to measure. The main advantages of Humicap includes high sensitivity, fast response, low hysteresis humidity, etc. In the upper-air sounding, when the ambient temperature is below -30 °C, water diffusion becomes quite difficult to film in the humidity, as a result, the response speed and accuracy will be reduced. The principle diagram of dual heat humidity sensor heating is given in Figure 1, which is constituted by four layers including the measuring humidity level, the measuring temperature level, the heating level and the substrate level. The dual heated humidity sensor consists of two humidity sensors with humidity sensors automatically rotate two alternate work. When humidity sensor A is heating, sensor B measures the humidity. When A completed the heating to measure, B switch heated.

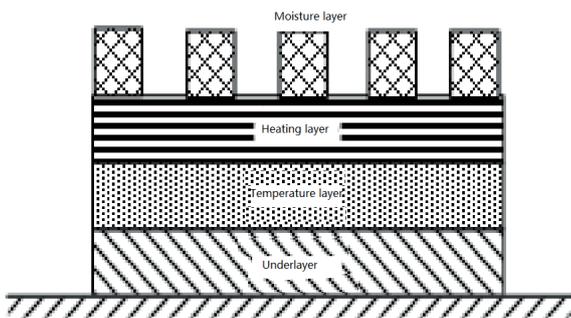


Fig. 1. Sensor heating principle structure

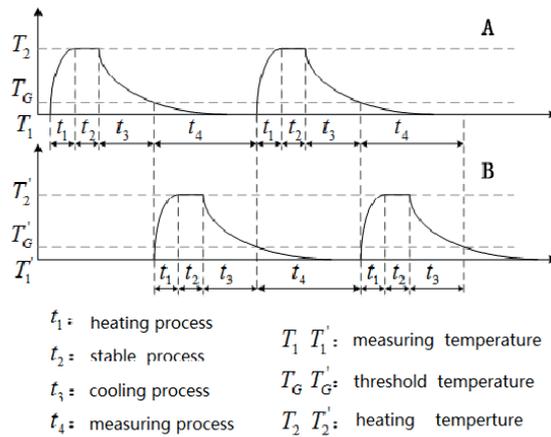


Fig. 2. The work process of pairs of heat and humidity sensors

As shown in Figure 2, when dual heating and humidity sensors are heating alternately, the measurement cycle can be simply divided into heating link t_1 , stable link t_2 , cool link t_3 and measuring link t_4 . Heating the plate in the heating part of the humidity sensor brings a temperature rise from ambient temperature T_1 to a target temperature T_2 . During the stable process, the temperature of the sensor at T_2 is maintained by the heating resistance in the chip. In the cooling part, the sensor is cooled by natural convection. Finally, the humidity is measured in the measurement part. Select the variability in Y-axis direction as the temperature drop threshold criteria T_G , when the temperature is lower than value of T_G , it will be similar to that temperature will not change. Therefore, the cooling process is divided into cool link and measurements link.

Interdigital sandwich structure is used in the layer of measuring wet. This structure increases the capacitance values of wet sense capacitance and the sensitivity of sensor. In the middle of the electrode, polyimide film is taken as Humicap media. According to the semi-empirical relationship of Looyenga:

$$\epsilon = \left[V(\epsilon_2^{1/3} - \epsilon_1^{1/3}) + \epsilon_1^{1/3} \right]^3 \quad (1)$$

where ϵ , ϵ_1 and ϵ_2 are complex, PI is the dielectric constant of water, V is the volume percentage of PI-absorbent that is related to RH. Greater the humidity would result in more adsorbed water molecules by the PI film. Besides, the greater the V , the greater the dielectric constant ϵ .

Then, the capacitance value of the humidity sensor is:

$$C = \frac{A\epsilon_0\epsilon_r}{d} \quad (2)$$

In this formula, C is the total capacitance value, d is the thickness of the dielectric film polyimide and ϵ_1 is a dielectric constant of the polyimide depending on humidity variations.

ESTABLISHING HEATING MODEL

THE EXPANSION RESPONSE CURVE METHOD

The size of the humidity sensor selected in this paper is 6 mm × 4 mm × 0.625 mm. Two titanium material heating plate is integrated on the heating layer, with the length, width and thickness are 5200 μm, 400 μm and 200 nm, respectively. When the sensor is added to the measurement circuit at a constant voltage 9 V, the measured sensor temperature T and the heating time t is shown in Figure 3.

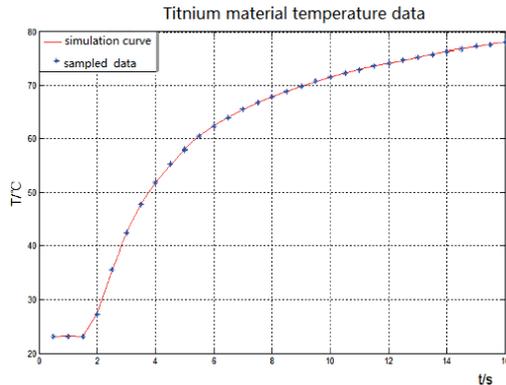


Fig. 3. Sensor temperature versus time curve

As shown in Figure 3, the heating process of the sensor can be approximately expressed by a first-order inertia link and a pure lag link, which is

$$G(s) = \frac{Ke^{-Ts}}{T_s + 1} \quad (3)$$

where, K is a static gain, T is the equivalent time delay, τ is the equivalent time constant. The unit step response is shown in Figure 2 (a). The parameter K can be determined by the ratio of output and input in the steady-state. τ and T can be calculated by a simple way based on the area of measurement according to equation (4):

$$\begin{cases} T + \tau = \frac{A_{01} + A_{02}}{k} \\ T = \frac{eA_1}{k} \end{cases} \quad (4)$$

Where A_{01} , A_{02} and are area which can be measured by Figure 4.

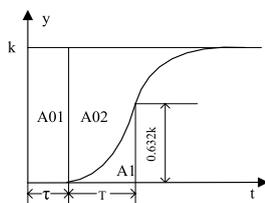


Fig. 4. The model parameters determined by Ziegler and Nichols method

ESTABLISHING HEATING MODEL

According to experimental data, K = 46, T = 2.8, $\tau = 1.2$ can be obtained using the expansion response curve. Thus, the transfer function $G(s) = \frac{46e^{-1.2s}}{2.8s + 1}$ can be determined for the heating plate, with the frequency characteristic given in Figure 5.

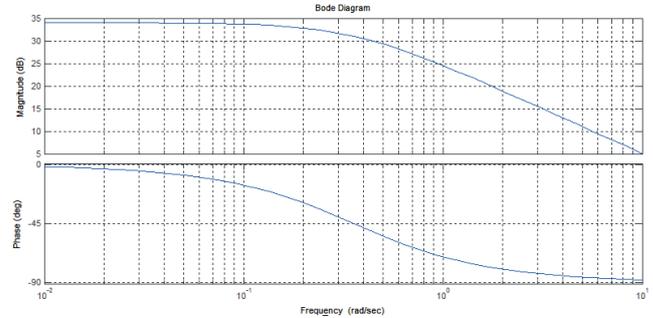


Fig. 5. The frequency characteristics of humidity sensor heating control system

Figure 5 can be obtained from the frequency characteristics of the system. The amplitude stability margin is $+\infty$, phase stability margin is -90° . When the humidity sensor heating plate open-loop frequency characteristic is greater than 0 dB logarithmic frequency domain, the number of phase curve for the -180° line crossing the both positive and negative is 0, so the closed-loop system is stable.

THE IMPLEMENTATION OF CONTROL ALGORITHM

PREDICTION MODEL

DMC Algorithm is a step response model of the system as a predictive model. When coupled with an input of the system step response, the sampling time at the $t = T, 2T, 3T, \dots, NT$ can be measured separately a sequence of sample values at the output of the system, with dynamic coefficients represented as $a_1, a_2, a_3, \dots, a_N$. Where N is the cut-off point of the step response, which is called the length of the time domain model. The choice of N should make a_i ($i > N$) close to its steady state value a_∞ . In proportion to the additive nature of the linear system and the use of this model, the output in the future of the system can be predicted according to the input control increment. The prediction model is given in equation formula (5)

$$\tilde{y}_{PM}(k) = \tilde{y}_{P0}(k) + A\Delta u_M(k) \quad (5)$$

where,

$$\tilde{y}_{PM}(k) = \begin{bmatrix} \tilde{y}_M(k+1|k) \\ \vdots \\ \tilde{y}_M(k+P|k) \end{bmatrix} \quad \tilde{y}_{P0}(k) = \begin{bmatrix} \tilde{y}_0(k+1|k) \\ \vdots \\ \tilde{y}_0(k+N|k) \end{bmatrix} \quad \Delta u_M(k) = \begin{bmatrix} \Delta u(k) \\ \vdots \\ \Delta u(k+M-1) \end{bmatrix} \quad A = \begin{bmatrix} a_1 & 0 & \dots & 0 \\ a_2 & a_1 & \dots & 0 \\ \vdots & \vdots & \dots & \vdots \\ a_p & a_{p-1} & \dots & a_{p-M+1} \end{bmatrix}$$

Here, P is the prediction domain length. Generally, $M \leq P \leq N$, where M is the control horizon length, and N is the length of the time-domain model.

ROLLING OPTIMIZATION

DMC is a control strategy algorithm based on optimization. At sampling time $t = kT$, the optimization performance index is given by formula (6),

$$\min J(k) = \sum_{i=1}^P q_i \left[\omega(k+1) - \tilde{y}_M(k+i|k) \right]^2 + \sum_{j=1}^M r_j \Delta u^2(k+j-1) \quad (6)$$

Where q_i and r_j are the weight coefficients.

At different times, the optimization performance indicators are not the same, but their relative forms are consistent. The so-called "rolling optimization" refers to the optimization time-domain goes forward with time constantly. Introducing vector and matrix notation as $w(k) = [w(k+1) \dots w(k+P)]^T$ and $Q = \text{diag}(q_1, \dots, q_p)$, $R = \text{diag}(r_1, \dots, r_M)$, then the optimization performance index of formula (6) can be rewritten as,

$$\min J(k) = \left\| \omega_p(k) - \tilde{y}_{PM}(k) \right\|_Q^2 + \left\| \Delta u_M(k) \right\|_R^2 \quad (7)$$

Where, Q and R are error weighting matrix and control matrix.

Without considering the input and output constraints, the time at $t = kT$, $\omega_p(k)$ and $y_{p0}(k)$ are both known, so that J(k) can achieve the minimum $\Delta u_M(k)$ by taking the extreme conditions necessary $dJ(k)/d\Delta u_M(k)$

$$\Delta u_M(k) = (A^T Q A + R)^{-1} A^T Q (\omega_p(k) - \tilde{y}_{p0}(k)) \quad (8)$$

FEEDBACK CORRECTION

Because of the model error, weakly nonlinear characteristics and other uncertain factors that exist in the actual process, the open-loop optimal control formula (8) based on prediction model equation (5) does not necessarily guarantee a system output following closely to the expectations. Moreover, the object being disturbed can not be taken into account. Therefore, we should use the error information in time during this process to correct the predicted value of output, instead of waiting until the M controls are implemented and making incremental correction. Therefore, the output of the system should be on the basis of output of predicted model, and use the actual output error correction, namely

$$\tilde{y}_{cor}(k+1) = \tilde{y}_{N1}(k) + h e(k+1) \quad (9)$$

Where

$$\tilde{y}_{cor}(k+1) = \begin{bmatrix} \tilde{y}_{cor}(k+1|k+1) \\ \vdots \\ \tilde{y}_{cor}(k+N|k+1) \end{bmatrix} \text{ is the output at } t = (k+1) \text{ (} i = 1, \dots, N \text{)}$$

of predicted system after error correction at $t=(k+1)T$. $h = [h_1, h_2, \dots, h_N]^T$ is the vector of error correction, where $h_1=1$, $e(k+1)$ is prediction error.

ANALYSIS OF SIMULATION RESULTS

From the angel of fluid dynamics (CFD) simulation that when the two humidity sensors are separated by more than 3 mm, it will not affect the temperature and humidity around the field of another when a sensor is heating, which means the measurement is valid in this case, the low- altitude mode and high-altitude mode are proposed in this paper. Specially, at the low-altitude mode (0 ~ 20 km), when the power is 0.6 W and the temperature rise is 46 °C, the surface temperature rise time is 5.8 s. On the contrary, at the high- altitude mode (20 km ~ 30 km), when the power is 0.4 W and the temperature rise is 40 °C, the high-altitude rise time is 5.8 s.

Sensor in the rising process and not in a straight line rise, in order to make the model more close to the real joined the cross wind effects of simulated rotation rising effect. At the same time, the sensor fully contact with the air. Due to the actual situation, the size of the sensor spacing of pitch angle research will not affect the study. Therefore, the final selected spacing is 3.5 mm, sea level and climatic conditions, pitch angles in Figure 6 are in 35°,40°,45° and 45° as the research object. Because of frictional resistance to the wall cutting area to be the force, and the wall boundary layer flow solver, the sensor and the air full contact friction, the larger inevitable, so use the model of wall shear should force (shear stress) as the reference variable.

Figure 6 shows cloud image of wall shear stress of the two sensors at a distance of 3.5 mm. From Figure 6 (a) available sensor surface shear stress 0.375 Pa, on its boundary is part of the region have different values. With the shear stress 0.432 Pa, sensors in Figure 6 (b) have different changes and the sensors of the shear stress distribution is different. In Figure 6 (c), surface shear stress distribution is uniform and the edge changes are also approximate symmetrical. Figure 6 (d) reveals a sensor surface shear stress change slowly, when humidity measurement error is larger.

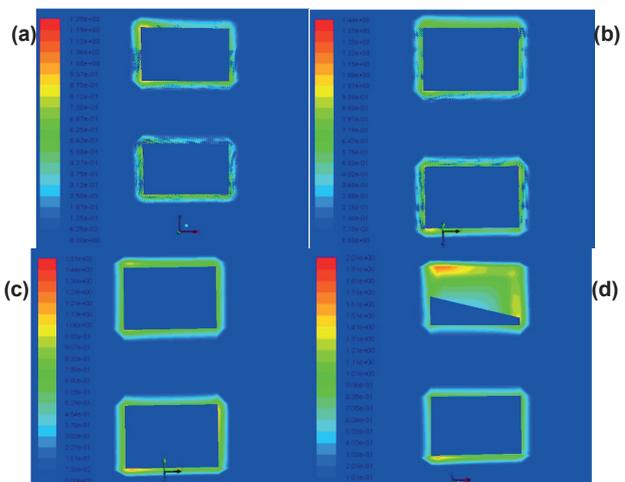


Fig. 6. Angle simulation diagram (a) pitch angle of 35° (b) pitch angle of 40° (c) pitch angle of 45° (d) pitch angle of 50°

When the sensor spacing is 3.5 mm, pitch angle is 45°, from the XY scatter diagram of the numerical distribution of the two sensors are more coincident, by the resistance of the air is basically the same, distribution interval of 0.1~1.7 Pascal, due to the presence of larger jump numerical variations, in addition to this part mainly concentrated in the 0.6 ~ 1 Pascal, the sensor surface shear should force change range is small and the values are pitching angle of 45°, 40° large on the boundary, as shown in Figure 7. Therefore, the choice of pitch angle, rolling angle and yaw angle are 45°, 90°, and 0°, respectively.

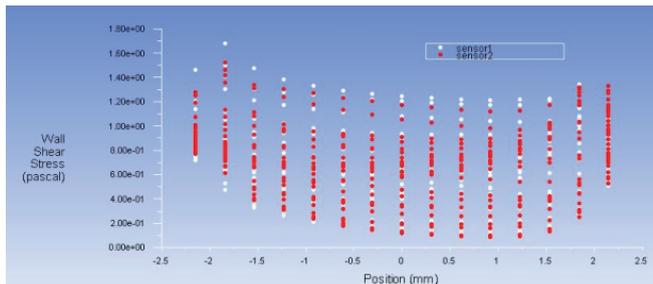


Fig. 7. Shear stress distribution in the wall of the pitching angle 45 degrees

Based on the control requirements discussed above, when the heating plate temperature rose from 0 °C to 46 °C, sampling period is taken as 20 s. The predictive control parameters were chosen as $T_s = 5, P = 10, M = 1, N = 30, \alpha = 2$. The value of system output feedback coefficient is $h = [h_1, h_2, \dots, h_N]^T$, and $h_1 = 1$. Because the system is a first-order inertial system, weighting matrix Q and R may be selected in accordance with the $Q = I$ (Unit matrix), to determine R in the real-time control process. The step response output curve of the system is shown in Figure 10.

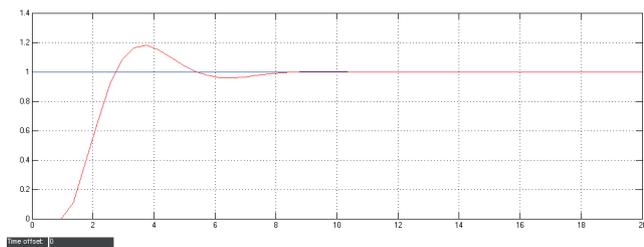


Fig. 8. PID temperature control heating film simulation results

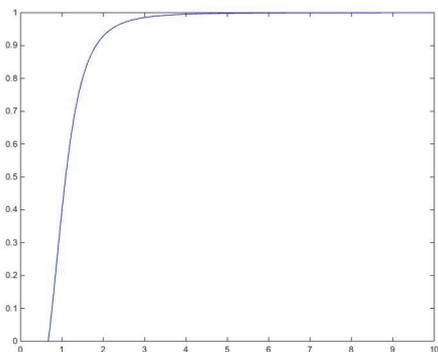


Fig. 9. Fuzzy temperature control heating film simulation results

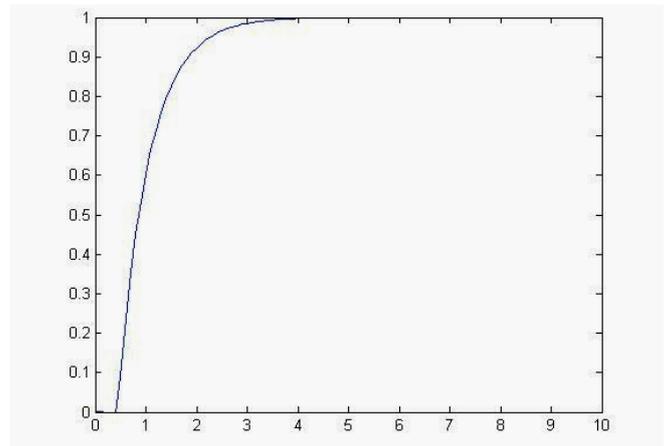


Fig. 10. DMC heating plate temperature control simulation results

The results of simulation shows that the control of DMC is faster than PID control (smaller overshoot, and settling time $t = 3.6$ s), which meets the heating requirements of low-altitude mode. Considering the limit conditions, high altitude heating model is difficult to establish, and the time of sensor response is very long (60 to 200 seconds) in the following -60 °C. Cooling time after heating is long at low pressure. Water in the cloud exists in the form of small ice crystals at this point, which means frost is less likely to generate on the sensor surface, therefore the heat treatment cannot be finished.

CONCLUSION

This paper studied the heating control process of dual heated sounding humidity sensor and built the relationship between the temperature and humidity, with its stability analyzed in details. DMC, Fuzzy and PID were used to control, heating and simulate. Results show that the control method in this paper has great stability, with stabilization time determined as 3.6 s, which meets the requirements of sounding humidity measurement. However, the model is relatively easy with some simplifications: since the heating layer is very thin, temperature of measurement temperature layer is considered to be equivalent to measurement humidity layer. The physical properties of the sensor itself is ignored after heated, which is also a hot point and difficult point of MEMS. In future studies, the model will be refined to make it better to meet the timeliness and accuracy of the altitude humidity detection.

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