Synthesis, characterization and analytical applications of chelating resin containing orcinol

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A chelating resin based on Salicylic acid-Formaldehyde copolymer, containing Orcinol (SFO), has been synthesized and characterized on the basis of Elemental Analysis, Particle Size Distribution, FT-IR Analysis, XRD, SEM and Optical Photographs. The Physico-Chemical properties have been studied. This resin is highly stable in acidic and alkaline solutions and has been studied as a chelating sorbent for heavy metal ions and transition metal ions. The Exchange capacity order is Ni(II) > Cu(II) > Zn(II) > Cd(II) > Pb(II). The effect of nature and concentration of different electrolytes on distribution coefficient (K_d) for metal ions have been investigated. Separation of synthetic mixtures containing Cu(II)-Pb(II), Ni(II)-Cd(II) and Brass constituents has been carried out using a column prepared from the synthesized chelating resin. The developed procedure was also tested for the removal of Cd(II) and Pb(II) from natural water of Purna River near by Navsari, Gujarat, India.

Keywords: Analytical Separation, Chelating Resin, Column Operation, Copolymer, Exchange Capacity.

INTRODUCTION

Water pollution is a major environmental problem faced by modern society that leads to ecological disequilibrium and health hazards¹. Metal ions such as copper, cadmium, lead, nickel and chromium often found in industrial wastewater, exhibit acute toxicity to aquatic and terrestrial life, including humans. Thus, the discharge of effluents into the environment is a chief concern. Many separation techniques using solvent extraction and ion exchange chromatography have been applied for this purpose. Ion exchange is a popular method owing to its applicability to both preconcentration and separation^{2,3}.

Park and Kim⁴ synthesized chelating resins containing carboxylic acid by suspension polymerization of styrene, methyl methacrylate and divinylbenzene in the presence of toluene. These resins were demonstrating good affinity for heavy metal ions like Pb(II), Cd(II) and Hg(II). A novel chelating copolymer resin was synthesized through the copolymerization of o-aminophenol and melamine with formaldehyde (o-APMF resin)⁵. This resin was useful for the separation and recovery of Pb(II) from synthetic binary mixtures of some metal ions. Singh and Srivastava⁶ prepared a chelating resin by condensing p-bromophenyl - hydroxamic acid, formaldehyde and salicylic acid and used this resin for the removal and recovery of Cu(II) and Fe(III) from synthetic seawater. The removal, separation and recovery of heavy metal ions from industrial wastewater have been a significant concern in all industrial branches owing to economic and environmental factors. Separation techniques such as ion exchange, solvent extraction, extraction chromatography, electodeposition, solid phase extraction and coprecipitation have been successfully used for the separation and preconcentration of several metal ions^{7,8}.

The aim of this article is to study the ability of chelating resin that contains hydroxyl and carboxylic acid groups as active sites. The chelating resin was synthesized from salicylic acid, formaldehyde and orcinol (SFO). This resin was characterized by different instrumental technique. The optimum condition for the efficient exchange of metal ions on synthesized resin was determined by varying contact time, pH and metal ion concentrations. The effect of salts like NaCl, Na_2SO_4 , $NaNO_3$ and tartaric acid on distribution coefficient (Kd) was investigated. Using this resin, the quantitative separation of Cu(II)-Pb(II) and Ni(II)-Cd(II) were achieved on the columns of the chelating resin. The chelating resin has also been studied for the separation of Cu(II) and Zn(II) from Brass sample and recovery of Pb(II) and Cd(II) from Purna river water.

EXPERIMENTAL METHODS

Reagents and Solutions

Analytical reagent (A.R) grade chemicals were used unless otherwise stated. Stock solutions (1g/L) of metal ions were prepared by dissolving appropriate amounts of metal acetate in deionized water, acidified with 5 mL of the corresponding acid. The working solutions of metal ions were obtained by dilution of the stock solutions with double distilled water. The solutions were adjusted to various pH using acetate buffer. The water samples from the Purna River (Navsari, Gujarat, India) was collected, acidified with 2% HNO₃ immediately, filtered and stored in the glass bottles. The Solutions of hydrochloric acid, tartaric acid, acetic acid, sodium acetate and sodium hydroxide were prepared by dissolving appropriate amount of the particular compound in double distilled water. All solutions were standardized by the literature methods^{9,10}.

Instrumental Analysis

A flame atomic absorption spectrophotometer (AAS) (Electronic Corporation of India Ltd, Hyderabad, India, Model 4129) with an air-acetylene flame (air and acetylene flow rates: 10 L/min and 2.0 L/min, respectively) was used for analysis. The wavelength (nm) used for the monitoring of Ni, Cu, Zn, Cd and Pb are 232.0,

324.8, 213.9, 228.8 and 217.0 respectively. The particle size of the synthesized resin (SFO) was measured by the "Malvern particle size analyzer" (Mastersizer-2000). The elemental analysis was carried out on the "Elemental Analyser" (Carlo Erba, model 1160). The FT-IR Spectra of the synthesized resin sample had been scanned in the KBr pallets on "FTIR Spectrophotometer" (Shimadzu model-8201PC). The X-Ray Diffraction Analysis (XRD) was performed by the advanced "Diffractometer" (Bruker AXE D8). The surface analysis was done using an optical photograph (Olympus SZX12) and a scanning electron microscope (Philips XL30) at different magnifications. A mechanical shaker equipped (speed of 200 strokes min-1) with an incubator (Hindustan Scientific, New Delhi, India) was used for the equilibration of metal ions with chelating resin.

Resin Synthesis

The recrystallised salicylic acid (0.1 mole, 13.7g) was ground to a fine powder and dissolved in 30 mL DMF solvent to give a clear solution. It was taken in a 250 mL three necked round bottom flask which was fitted with a condenser, a thermometer, and an addition funnel. Formaldehyde (37% w/v, 0.3 mole) was added to the above solution from the addition funnel dropwise with constant stirring. A solution of orcinol (0.1 mole, 12.4g) in 20 mL of DMF was added to the above solution funnel at room temperature and stirred for 1 hour. The mixture was refluxed on a water bath with constant stirring at $80\pm2^{\circ}$ C for 45–60 minute until a viscous solution was obtained with the formation of a jelly mass of dark brown color resin.

This jelly mass then dried in open to soft solid mass. It was ground to small pieces. The resin was cured in an oven at 70–75°C for 12 hour. The resin particles were washed with DMF and ethanol and finally with hot distilled water till the complete removal of monomer impurities was achieved¹¹. After a complete washing cycle, the yield of this resin was found to be 70–80% (18–20 g). The solubility tests of the resin were performed at room temperature with intermittent shaking. It was found insoluble in all common organic solvents like acetone, ethanol, benzene, DMF, DMSO, CCl₄, chloroform etc. and all acids and alkalies of higher strengths. As carboxylic acid groups normally get decomposed above 100°C. The resin was cured below 90°C.

The purified and dried resin sample (SFO) was finely ground and sieved to the obtained uniform particle of 20–50 mesh size and stored in a polyethylene bottle. The sieved resin sample was analyzed for particle size distribution. The structural and surface morphology of dry resin samples were examined by elemental analysis, FTIR spectra, XRD analysis, optical photograph and SEM analysis. The probable unit structure and the reaction scheme are given in Scheme 1.

The resin sample having uniform particle size (20–50 mesh) was equilibrated with 2M HCI solution for 24 hours to convert it in H^+ form and washed with deionized water till it was freed from chloride by testing with silver nitrate solution. The H^+ form of resin was used for further studies. It is necessary to evaluate ion exchange processes in terms of resin properties such



Scheme 1. Reaction Scheme for synthesized resin

as % moisture content, void volume fraction, exchange capacity for sodium ion and other heavy metal ions^{9,10}.

Effect of Contact Time on Exchange Capacity

To study the effect of important parameters like contact time, pH, metal ion concentration and temperature, batch equilibration method has been adopted at room temperature $(30\pm2^{\circ}C)$. To study the effect of contact time on the exchange of metal ions, H⁺ form of accurately weighed $(0.250\pm0.001 \text{ g})$ dry resin sample was taken in different glass stopper bottles and equilibrated with buffer solutions of optimum pH value (pH of which highest ion exchange capacity is observed) for 6 h. After decanting buffer solution, 50 mL (500 ppm) metal ion solutions of the same pH was added. The amounts of residual metal ions were determined by Atomic Absorption Spectroscopy at fixed time intervals. The exchange capacity was determined by the following equation:

$$q_e = \frac{(Co - Ce)V}{W} \tag{1}$$

Where Co and Ce are the initial and equilibrium concentration of metal ions in the aqueous phase respectively and V is volume of metal ion solution in mL and W is weight of resin in gram.

Effect of pH on Exchange Capacity

To study the effect of pH on the metal ion uptake, it is necessary to buffer the resin and then the solutions were used. Different sets of accurately weighed (0.250 ± 0.001) g) dry resin having uniform particle size (20-50 mesh) were equilibrated with buffer in different glass stopper bottles for 6 h, so that resin attained desired pH value. After 6 h, buffer solutions were decanted and 50 mL of 500 ppm metal ion solutions of varying pH from 3-7 were added. Metal ion solutions were equilibrated at room temperature (30±2°C) for 24 h with intermittent shaking. After 24 h, the solutions were filtered with 0.02 μ m membrane filter to separate the resin and solution. The pH of the filtrate was measured and it was found that pH remains stable throughout the experiment (± 0.2) . From the filtrate the unchelate metal ions were estimated by atomic absorption spectroscopy.

Effect of Metal Ion Concentration on Exchange Capacity

To study the effect of metal ion concentration by the synthesized resin, the accurately weighed $(0.250\pm0.001 \text{ g})$ dry resin was equilibrated with acetate buffer at desired pH values (pH value of highest exchange) for 6 h and then buffer solutions were decanted and metal ion solutions (50 mL) of varying molar concentration i.e. 100–500 ppm of the same pH value were added and equilibrated at room temperature for 24 h with intermittent shaking. After 24 h metal ion solutions were estimated.

Effect of Temperature on Exchange Capacity

To study the effect of temperature equilibration experiments were performed at fixed metal ion [Cu(II)] concentration (300 ppm) for fixed resin loading $(0.250\pm0.001$ g) and optimum pH at four different temperatures i.e. 30, 40, 50 and 60°C for 8 h.

Effect of Different Electrolytes Concentration on Distribution Coefficient (Kd) of Metal Ions

The dry resin sample $(0.250\pm0.001 \text{ g})$ was suspended in the different electrolyte solution like tartaric acid, NaCl, NaNO₃ and Na₂SO₄ (50 mL) of different known concentrations. The pH of the suspension was adjusted to the desired value and the resin was equilibrated for 6 h. To the suspension, 2.0 mL of (5.0 mg/mL) solution of the metal ion under study was added. The pH was again adjusted to a desired value. The mixture was further equilibrated for 24 hours and then filtered. The solid was washed with water. The filtrate and washings were combined and examined for the metal ion concentration.

 $K_{d} = \frac{\{ \text{Wt.} (\text{in mg}) \text{ of metal ions taken up by } 1 \text{ g of resin} \}}{\{ \text{Wt.} (\text{ in mg}) \text{ of metal ions present in } 1 \text{ mL of resin} \}}$ (2)

Analytical Column Separations

The chelating resin in H⁺ form was equilibrated at the desired pH and packed into a chromatographic column to form a bed 17 cm height and 0.4 cm diameter. Mixtures of metal ions (10 mg of each per 20 mL) at appropriate pH were passed through the column at a flow rate of 0.5 mL/min. The chelated metal ions were eluted using tartaric acid. During the elution, a flow rate of 0.5 mL/min was maintained.

Separation of Metal ions from Brass Sample

Brass is an alloy containing 60% Cu and 40% Zn. Brass sample $(0.250\pm0.001 \text{ g})$ was dissolved in about 10.0 mL of concentrated nitric acid and the solution was evaporated to dryness. The residue was dissolved in 10.0 mL of 0.1 M hydrochloric acid. The solution was filtered and made it up to 25.0 mL by addition of distilled water in standard measuring flask. From this, 5.0 mL of the solution was taken for column separation. This aliquot was directly passed through the column of the synthesized resin at a flow rate of 0.5 mL/min.

Recovery of Heavy Metal Ions from Purna River Water

20 liter of Purna River water sample from Navsari city was collected in a polythene container. Several water samples were analyzed to contain Cd(II) (0.01 to 0.17 ppm) and Pb(II) (0.01 to 0.4 ppm), which is higher than the Indian Standard Desirable Limits. It exhibits higher

concentration of these metal ions at Jalalpor and Weircum Causeway. This may be due to industrial effluent of sewage waste in the river water. One liter of water sample was recycled through the resin columns for the preconcentration of these metal ions at a flow rate of 1 mL/min. The elution was performed at optimized condition based on K_d values.

RESULT AND DISCUSSION

Instrumental Analysis

The particle size distribution curve is shown in Figure 1. The particle size for resin is quite homogeneous. The average particle size of resin is found to be in the range of 250–850 micrometer (20–50 mesh). It provides the optimum size for the exchange of the ions and also comparable with the commercial resins.



Figure 1. Particle size distribution curve of SFO resin

The %C, %H and %N was calculated by from the general formula $(C_{15}H_{12}O_5)$ of the repeating unit of the assumed structure (Scheme 1) of the synthesized resin. The result of the elemental analysis is in good agreement with calculated values of C, H and N, which is shown in Table 1. The values of Elemental Analysis confirm the proposed structures of the resin presented in Scheme 1.

 Table 1. Elemental analysis and Physico-chemical properties of SFO resin

Properties	Value		
%C Calculated (Found)	66.17 (66.53)		
%H Calculated (Found)	4.41 (4.79)		
% Moisture	3.11		
% Solid	96.89		
True density (d _{res}) (g/cm ³)	1.111		
Apparent density (d _{col}) (g/ml)	0.740		
Void volume fraction	0.333		
Sodium Exchange Capacity (mmol/g dry resin)	4.948		
Concentration of fixed ionogenic group (mmol/cm ³)	5.260		
Volume capacity (mmol/cm ³)	3.508		

The strong band at 3414.36 cm⁻¹ for resin is due to the v (O-H) stretching of phenolic group. The presence of the medium band at 2942.87 cm⁻¹ for resin is due to the v(C-H) stretching of methylene group¹². The medium strong band at 1652.81 cm⁻¹ for resin can be assigned to v(C=O) stretching of aromatic acid group. The medium band at 1099.38 cm⁻¹ for resin which is due to the δ (C-H) bending of 1, 2, 3, 5-tetra substituted benzene ring. The medium band at 1466.52 cm⁻¹, 760.15 cm⁻¹, 1376.12 cm⁻¹ for resin is due to the δ (C-H) bending, δ (C-H) rocking, δ (C-H) wagging of ethylene (-CH₂-) bridges, which can be observed in Figure 2.



Figure 2. FTIR spectra of SFO resin

The XRD patterns of the compound provide the information about the crystalline or amorphous nature of the compound or crystalline and amorphous regions that may co-exist in the same compound^{13,14}. The XRD pattern of resin is shown in Figure 3. Some very few sharp peaks are observed in the difractograms of resin. The resin exhibits characteristic of the low percentage of crystalline nature with an amorphous phase.

Surface analysis has found great use in the understanding of the surface features of the material. The morphology of the synthesized resin sample was investigated by scanning electron micrographs and optical photographs. The SEM photographs are shown in Figure 4 at (a) 200X and (b) 1000X magnifications and optical photographs are shown in Figure 5 (140X–220X). The white bar at the bottom of the SEM micrographs represents the scale. SEM and optical photographs of SFO resin sample was taken to characterize particle shape, size and surface morphology. From the SEM photographs, (Figure 4) it is observed that resin exhibits angular edges with regular fringes. The morphology of the resin shows a fringed micelle model of the crystalline structure. The fringes represent the transition material between crystalline and amorphous phases. The SEM photographs of resin exhibits such spherulites, which are the aggregate of crystallites present in the amorphous regions. SFO resin has more amorphous region as compare to *o*-APMF resin⁵. The synthesized resin is more compact and rigid. Optical photographs (Figure 5) of the synthesized resin exhibit that the resin is dark brown in color.

Physico-Chemical Properties

The physico-chemical properties of the synthesized resin are presented in Table 1. The percentage of moisture content of the synthesized resin is 3.11. It has been observed that this resin has low range of percentage moisture content compared to the commercial resins. The amount of cross linking in the bead has an impact on the moisture content of the bead and the moisture content in turn has an impact on the selectivity. A bead with high moisture content has a high porosity and the active groups are spaced further apart from each other. The resin synthesized from salicylic-formaldehyderesorcinol¹⁵ and salicylic acid-formaldehyde- m-cresol¹⁶ exhibited higher moisture content than the synthesized resin (SFO). The difference in the moisture content may be due to the different experimental conditions such as the medium in which the resins are synthesized, polymeric



Figure 3. XRD pattern of SFO resin









[a]

Figure 5. Optical photographs of SFO resin at [a] 140X and [b] 220X magnification

backbones and functional groups involved.

The true density of the synthesized polymer is shown in Table 1 which is 1.11 g/cm³. The true density of commercial resins generally lies between 1.1g/cm3 to 1.7 g/cm³. To avoid the floating of resin particles, true density must be more than one. The apparent density of the synthesized resin is 0.740 which is given in Table 1, which is comparable to the density of commercial resins. It may be because of charge in polymeric matrix, different functional group and the method of synthesis. The apparent density parameter gives an idea of probable length of the packed column for an ideal column chromatography study. The value of void volume fraction of resin is 0.333 which is represented in Table 1. The appreciable values of void volume fraction help the diffusion of the exchangeable ion on the resin and hence increase the rate of the exchange of ions.

Effect of Contact Time on Exchange Capacity

The exchange of metal ions on resin exhibits the time dependent phenomenon. The rate of exchange for different metal ions is illustrated in Figure 6. The graph shows that the time required for 50% exchange (t_{12}) of Ni(II), Cu(II) and Zn(II) is 30 min., for Cd(II) is 40 min. and for Pb(II) is 50 min. The faster rate of exchange in the beginning can be explained on the basis of the law

of mass action¹⁷. The faster rate of exchange facilitates column chromatographic separation. The kinetics of metal ion exchange mainly depends on the various physical properties like particle size distribution, pore size, physical core structure and diffusion of counter ion. The time required for 100% uptake of metal ions was 21 hr.

Effect of pH on Exchange Capacity

The polymer surface chemistry as well as the solution chemistry of these metal ions is pH dependent. Changes in pH are known to affect the adsorbent's surface charge and the adsorbate's degree of ionization and speciation¹⁸. The result is presented as the exchange capacity against pH for the metal ions in Figure 7. The maximum exchange for Ni(II) and Cu(II) take place at pH 6.0 and for Zn(II), Cd(II) and Pb(II) at pH 5.0. The results show that the exchange of metal ions was increased with the increase in pH up to a certain value and thereafter it decreased. An increase in pH increases the negatively charged nature of the sorbent surface. This leads to an increase in the electrostatic attraction between the positively charged metal ions and the negatively charged sorbent and results in the increase in the uptake of metal ions. The decrease in the removal of metal ions at lower pH is due to the higher concentration of H⁺ ions present in the reaction mixture which



Figure 6. The effect of pH on metal ion exchange capacity on SFO resin



Figure 7. The rate of exchange for metal ion exchange capacity on SFO resin

compete with the metal ions for the exchange sites on the sorbent surface. Meanwhile the observed decrease in the exchange at higher pH is due to the formation of insoluble hydroxide of the metal ions^{19,20}. From the nature of the trend observed it is indicated that the cation exchange behavior of this resin is similar to acidic cation exchangers^{4,19}.

The selectivity order for metal ions is Cu(II) > Ni(II)> Zn(II) > Cd(II) > Pb(II). The resin shows low exchange capacity for heavy metal ions as compared to other metal ions under study. The exchange capacity of Zn(II) is also found less as compared to other transition metal ions of 3d series. This can be explained on the basis of π bonding electrons. It is observed that metal chelate forming capacity for 3d series metal ions goes on decreasing from Cu(II) > Ni(II) > Zn(II), due to the less availability of n bonding electrons. The lower capacity of Zn(II) can also be explained by greater hydrated-ion radius of Zn(II) than that of Ni(II) and Cu(II) which leads to lower stability. The transition elements Cd(II) and Pb(II) of 4d series metal ions show less capacity. It is because of having greater hydrated ion radius than 3d series transition metal ions under study. This will results in electrostatic attraction between the metal and coordinating group, lower the complex stability and hence lower the capacity. The ion exchange capacity is also influenced by the morphology of resin, which in turn, is related to the different groups present in monomers.

Effect of Metal Ion Concentration on Exchange Capacity

The examination of the data presented in Figure 8 reveals that the amount of metal ion uptake increases with the increase in the concentration of metal ions in solution until a maximum value, and will remain constant



Figure 8. The efect of concentration on metal ion exchange capacity on SFO resin

upon further increase in metal ion concentration. At a lower concentration of metal ions, the number of metal ions available in the solution is less as compared to the available sites on the sorbent. However, at higher concentration the available sites of exchange remain same, whereas more metal ions are available for the exchange and subsequently the exchange becomes almost constant then after. For Ni(II), Cu(II), Zn(II) and Cd(II) after 300 ppm concentration ion exchange attains limiting value. For Pb(II) after 400 ppm concentration metal ion uptake becomes constant.

Effect of Temperature on Exchange Capacity

Thermal stability test gives significant information for cation exchange capacity of resin. When resin was heated for 30°C to 60°C for 8 h, it is observed that the Cu(II) exchange capacity remains unaltered. This may be due to cross linking between monomers, which produces tough resin. Resin shows little increase in the capacity at higher temperature. This is due to (1) the destruction of some $-CH_2$ - bridge between aromatic ring, and (2) removal of decomposed products had neutralized the ionogenic groups. The thermal stability of resin makes resin useful for ion exchange chromatography at high temperature.

Effect of Different Electrolytes Concentration on Distribution Coefficient (K_d) of Metal Ions

The distribution coefficient (Kd) of metal ions is function of concentration of different electrolyte solution. During the exchange of metal ions in the presence of electrolyte solution the difference in the distribution coefficient values is caused by the competition between metal ions and counter ions from electrolyte solution for the available exchange sites. To study the effect of electrolyte concentration on distribution coefficients of Ni(II), Cu(II), Zn(II), Cd(II) and Pb(II) ion, 0.05 to 1.0 M solutions of tartaric acid, sodium chloride, sodium nitrate and sodium sulphate were used. The result is given in Table 2. It is observed that the metal ion distribution coefficients go on increasing as the concentration of electrolyte decreases. It was observed that there is a pronounced difference in the distribution coefficient values of sodium chloride, sodium nitrite and sodium sulphate.

The exclusion of the electrolyte solution from the resin goes on increasing with decreasing electrolyte concentration and hence increase in the distribution coefficient is observed. The electrolyte exclusion is more efficient with counter ions of low valency and co-ions of high valency. Therefore in the table, it is observed that the distribution coefficients, of the metal ions in presence of sodium sulfate have higher values than those in the presence of sodium chloride and sodium nitrate and the lower K_d values observed in tartaric acid electrolyte, this may be due to the fact that the chelating group is available in tartaric acid.

The synthesized resin exhibits higher K_d values for Cu(II) and lower values for Pb(II). This may be explained on the basis of stability constant or the difference in the energy of the complexes according to Irving and Williams⁸. The value of the distribution ratio for the given concentration of electrolytes at optimum pH depends upon the nature and the stability of a chelate formation for particular metal ion. To achieve more clean separation of heavy metal ions in short time with practical elution volume, maximum (K_d) value difference was selected for optimized conditions of chromatography.

Table 2. K_d values of metal ions on SFO resin in different electrolyte at optimum pH

Metal ion	Concentration of electrolyte (M)	K _d values of electrolyte at optimum pH			
		Tartaric acid	Sodium Chloride	Sodium Nitrite	Sodium Sulfate
Ni(II) -	1.0	41.87	108.65	159.10	196.62
	0.5	77.09	142.58	188.70	232.49
	0.1	164.28	212.58	304.20	356.19
	0.05	189.70	252.38	342.10	378.21
Cu(II)	1.0	95.71	148.28	222.10	261.80
	0.5	138.31	176.91	259.42	284.18
	0.1	208.65	221.05	271.70	304.58
	0.05	312.89	288.42	376.17	438.61
Zn(II)	1.0	32.48	128.60	158.90	189.72
	0.5	80.04	152.91	174.88	199.10
	0.1	112.84	178.50	181.82	211.40
	0.05	149.50	184.38	204.90	242.67
Cd(II)	1.0	23.61	78.43	108.50	132.47
	0.5	49.12	87.58	122.70	155.10
	0.1	91.47	112.91	142.88	194.33
	0.05	109.24	138.04	177.60	223.10
Pb(II)	1.0	12.91	36.64	75.28	87.56
	0.5	29.06	58.25	92.70	103.83
	0.1	38.45	71.12	101.40	113.75
	0.05	47.84	88.41	118.70	126.78

Analytical Column Separations

The superior selectivity towards multivalent cations exhibited by chelating resin has been demonstrated in column experiments by using K_d value. The values of the K_d are shown in Table 2. An ideal situation would be such that one K_d value is ten times greater than the K_d value for the other ion, while the other approaches zero. The first eluting fraction of tartaric acid carries one metal ion, which has a smaller K_d value. The second metal ion can be eluted by changing the tartaric acid concentration to a level that has a lowest K_d value for second metal ion. The separation of Pb(II) from Cu(II) was carried out at appropriate condition. Pb(II) was eluted by 0.05 M tartaric acid at 5.0 pH. By changing concentration of tartaric acid (1.0M) at 6.0 pH, Cu(II) was eluted. The plot of eluted volume versus % of metal ion elution is shown in Figure 9. No cross contamination was observed for this separation. In separation of Cd(II) from Ni(II), Cd(II) was eluted by 0.05M tartaric acid at pH-5.0 and then Ni(II) eluted by 1.0 M tartaric acid at pH-6.0, which shown in Figure 10. The recovery of metal ions has been more than 90% in all cases. Synthesized resin was very useful for separation of metal ions particularly for heavy metal ions.



Figure 9. Separation of Cu(II) and Pb(II) on SFO resin



Figure 10. Separation of Ni(II) and Cd(II) on SFO resin

Separation of metal ions from Brass Sample

The separation of Cu(II) and Zn(II) from Brass Sample is carried out in the synthesized resin column. In the separation of Zn(II) from Cu(II), the resin column equilibrated at pH 6.0. Zn(II) was eluted with 0.5 M tartaric acid. The first few fractions contained only Zn(II)

and the later fractions contained only Cu(II) which was eluted with 1.0 M tartaric acid at pH 6.0. The plot of the eluted volume versus % of metal ion elution is shown in Figure 11. No cross contamination was observed for this separation. The recovery of Zn(II) and Cu(II) was more than 90%.



Figure 11. Separation of Zn(II) and Cu(II) of Brass Sample on SFO resin

Recovery for Heavy Metal Ions from Purna River Water

To verify the applicability of the present chelating resin using preconcentration of trace metal ions like Cd(II) and Pb(II) from river water sample, the extraction and elution of metal ions was studied. The metal ion concentration of Cd(II) and Pb(II), in river water and after preconcentration was determined by atomic absorption spectroscopy. The recovery of heavy metal ion from column was carried out using 2M HCl solution. The recovery of Cd(II) and Pb(II) ions was 90.47% and 92.11%. The results indicate that the extraction and elution of Cd(II) and Pb(II) is little affected by the coexistence of salt matrices.

CONCLUSIONS

The synthesized SFO chelating resin exhibits exchange capacities for metal ions which is pH hdependent. The Highest removal for selected metal ions occurred at 5.0 to 6.0 pH. The time required for 50% exchange (t_{12}) was mostly achieved in approximately 30 to 40 min. The exchange capacity of the transition metal ion is greater than that of heavy metal ion because of fewer pores and pits size on the surface of SFO resin. The present investigation shows that cation exchange resin (SFO) can be employed for separation and recovery of metal ion from their mixture. Batch and column methods were done for the separation of heavy metal ion from synthetic binary mixture. The recovery of metal ions from their mixture is about 90% using suitable eluents. This resin may be also used for wastewater treatment in industries. The use of chelating resin for the separation and removal of metal ions is the method of choice due to its high separation efficiency, good reproducibility of retention parameters and simplicity; therefore, this resin can be used in the enrichment of metal ions from various sources by adopting preconcentration and separation from various matrices.

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