

# Processing and microwave dielectric properties of $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$ ceramics

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$\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics was processed via solid state mixed oxide sintering route. X-ray diffraction revealed single phase formation of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics that crystallized into an orthorhombic crystal structure with a space group Pnnm with lattice parameters of  $a = 5.681 \text{ \AA}$ ,  $b = 32.542 \text{ \AA}$  and  $c = 3.968 \text{ \AA}$ , refined by the least squares method. The unit cell density ( $\rho_{\text{th}}$ ) was  $6.71 \text{ g/cm}^3$ . The microstructure consisted of plate-like grains and the average size was increased from  $2 \mu\text{m}$  to  $5 \mu\text{m}$  with an increase in sintering temperature from  $1450^\circ\text{C}$  to  $1575^\circ\text{C}$ . Optimum microwave dielectric properties, i.e.  $\epsilon_r \sim 66$ ,  $Q_u f_0 \sim 8500 \text{ GHz}$  and  $\tau_f \sim 180 \text{ ppm/}^\circ\text{C}$ , were achieved for  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics sintered at  $1550^\circ\text{C}$  for 4 h.

Keywords: *electron microscopy; sintering; microwave ceramics*

## 1. Introduction

Dielectric resonator (DR) is a key component in wireless telecommunication systems and it greatly reduces the size of the microwave components due to its high relative permittivity,  $\epsilon_r > 24$ ,  $Q_u f_0 > 30,000 \text{ GHz}$  and  $|\tau_f| \leq 3 \text{ ppm/}^\circ\text{C}$ , which are the necessary requirements for a material to be commercially used as DR [1]. However, the requirements for low  $\tau_f$  and high  $Q_u f_0$  are flexible for certain applications such as antennas [2].

$\text{A}_5\text{B}_5\text{O}_{17}$  family of layered perovskites has attracted great attention due to their good performance for patch antennas applications [3–5].  $\epsilon_r = 53$ ,  $\tau_f = -20 \text{ ppm/}^\circ\text{C}$  and  $Q_u f_0 = 17359 \text{ GHz}$  was reported by Jawahar et al. [6] for  $\text{CaLa}_4\text{Ti}_5\text{O}_{17}$  ceramics. Partial Zn substitution for Ca improved the microwave dielectric properties of  $\text{CaLa}_4\text{Ti}_5\text{O}_{17}$  ceramics [7].  $\epsilon_r = 57$ ,  $Q_u f_0 = 15,000 \text{ GHz}$ , and  $\tau_f = -8.16 \text{ ppm/}^\circ\text{C}$

were obtained for  $\text{Ca}_{0.99}\text{Zn}_{0.01}\text{La}_4\text{Ti}_5\text{O}_{17}$  ceramics with 0.5 wt.% CuO additive that were sintered at  $1450^\circ\text{C}$  for 4 h [8]. Isupov et al. [9] firstly reported  $\text{Sr}_5\text{Nb}_4\text{TiO}_{17}$  within  $\text{SrO-Nb}_2\text{O}_5\text{-TiO}_2$  ternary system.  $\text{Sr}_5\text{Nb}_4\text{TiO}_{17}$  adopt the centrosymmetric orthorhombic crystal structure with space group Pnnm, No. 58. Iqbal et al. reported [10]  $\epsilon_r \sim 80$  for  $\text{Sr}_5\text{Nb}_4\text{TiO}_{17}$  ceramics. Iqbal et al. investigated [11] the microwave dielectric properties and reported  $\epsilon_r \sim 74$ ,  $Q_u f_0 \sim 1303 \text{ GHz}$  and  $\tau_f \sim 332 \text{ ppm/}^\circ\text{C}$  for  $\text{Sr}_5\text{Nb}_4\text{TiO}_{17}$ . The high positive  $\tau_f$  of  $\text{Sr}_5\text{Nb}_4\text{TiO}_{17}$  precluded its application as DR. It has been reported that substitution of Nb with Ta reduced the value of  $\tau_f$  and improved the properties of microwave dielectric ceramics such as  $\text{Ba}_3\text{LiNb}_{3-x}\text{Ta}_x\text{Ti}_5\text{O}_{21}$ ,  $\text{Sr}_2\text{La}_3\text{Nb}_{1-x}\text{Ta}_x\text{Ti}_4\text{O}_{17}$ ,  $\text{Ca}_5\text{Nb}_{2-x}\text{Ta}_x\text{TiO}_{12}$ , and  $\text{Mg}_4\text{Nb}_{2-x}\text{Ta}_x\text{O}_9$  [12–15], however, as per my understanding and knowledge the effect of Ta substitution for Nb on microwave dielectric properties of  $\text{Sr}_5\text{Nb}_4\text{TiO}_{17}$  has not been investigated. Therefore, in this paper, the microwave dielectric properties of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  were investigated.

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## 2. Experimental

The initial ingredients:  $\text{SrCO}_3$  (Aldrich, 99+ %),  $\text{Ta}_2\text{O}_5$  (Aldrich, 99.95 %), and  $\text{TiO}_2$  (Anatas, Aldrich, 99+ %) were dried to remove the moisture before weighing in order to ensure the correct initial stoichiometry of the final ceramics. The dried carbonates and oxides were milled in polyethylene mill jars using Y-toughened  $\text{ZrO}_2$  balls as grinding media and 2-isopropanol as a lubricant to make freely flowing slurries for 24 h. The slurry was dried by the evaporation of 2-isopropanol from the slurry at 95 °C. The powder was then sieved before calcination at 1400 °C for 6 h, with a heating/cooling rate of 5 °C/min. The calcined powder was ground in a mortar with a pestle for about 45 min to dissociate the agglomerates. This fine powder was pressed into 10 mm diameter and from 4 mm to 5 mm high pellets at 100 MPa. The pellets were placed on platinum foils and sintered in a range of temperature of 1450 °C to 1575 °C for 4 h. Phase analysis of the sintered crushed pellets was carried using a Philips X-ray diffractometer operating at 30 kV and 30 mA at 1°/min at  $2\theta = 10^\circ$  to  $70^\circ$  with a step size of  $0.02^\circ$ . A STOE PSD X-ray diffractometer with  $\text{CuK}\alpha$  radiation ( $\lambda = 1.540598 \text{ \AA}$ ) was used for the measurement of lattice parameters. The bulk apparent densities of the sintered pellets were measured using Archimedes method. The percentage relative densities were then calculated by taking the ratio of unit cell density to the apparent densities for each sintered sample.

Each sintered pellet was cut and finely polished before thermal etching for 30 min at temperatures  $\sim 10\%$  less than its corresponding sintering temperature at a heating/cooling rate of 5 °C/min for microstructural examination. The etched surfaces of the samples were gold-coated to avoid charging effects and a JEOL 6400 SEM operating at 20 kV was used.

The faces of the optimally sintered pellet were coated with gold paste and heated to 800 °C for 2 h at heating/cooling rates of 10 °C/min. The dielectric properties were measured in the range of 1 kHz to 1 MHz using HP 4384 A LCR meter.

The microwave dielectric properties were measured using Advantest R3767CH Network Analyzer employing cavity method by placing the cylindrical pellets on a low loss quartz single crystal at the center of Au-coated brass cavity. The  $\tau_f$  was measured by noting the temperature variation of  $\text{TE}_{01\delta}$  resonance mode in the temperature range of 20 °C to 80 °C using equation 1:

$$\tau_f = (f_2 - f_1) / f_1 \Delta T \quad (1)$$

where  $f_1$  and  $f_2$  are the resonant frequencies at 20 °C and 80 °C, respectively, and  $\Delta T$  is the difference between the initial and final temperatures.

## 3. Results and discussion

The room temperature XRD pattern of the highest density sample of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics is shown in Fig. 1. The reflections were indexed according to PDF Card No. 87-1170 of  $\text{Sr}_5\text{Nb}_4\text{TiO}_{17}$ . Within the in-house XRD detection limit, the sample was formed as a single phase having orthorhombic crystal structure with a space group Pnnm. The red line pattern is the PDF Card No. 87-1170 and the green is our XRD pattern. The unit cell parameters were calculated from the XRD data using least squares method and are  $a = 5.681 \text{ \AA}$ ,  $b = 32.542 \text{ \AA}$  and  $c = 3.968 \text{ \AA}$ . Although  $\text{Nb}^{5+}$  and  $\text{Ta}^{5+}$  ions are of almost the same size [16], however, a small increase in the lattice parameters is observed for Ta based composition in comparison to Nb counterpart [11]. This slight increase in lattice parameter increased the cell volume and was found to be  $733.6 \text{ \AA}^3$ .

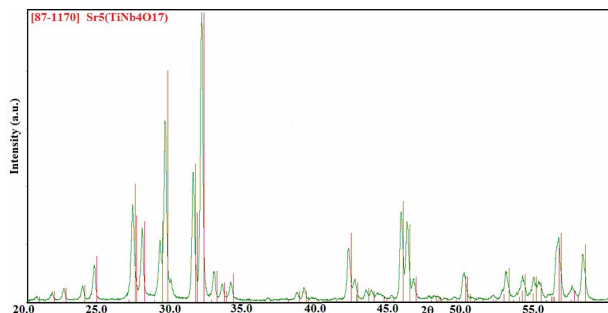


Fig. 1. XRD pattern of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics sintered at 1550 °C for 4 h.

The theoretical density  $\rho_{th}$  was calculated from the unit cell data using equation 2:

$$\rho_{th} = ZM/VA_g \quad (2)$$

where  $Z$  is the formula unit,  $M$  is the molecular weight,  $V$  is the volume of the unit cell and  $A_g$  is the Avogadro number. The  $\rho_{th}$  was obtained to be  $6.71 \text{ g/cm}^3$  which is larger than that of Nb counterpart ( $\text{Sr}_5\text{Nb}_4\text{TiO}_{17}$ ) for which  $5.15 \text{ g/cm}^3$  was reported [11]. The increase in  $\rho_{th}$  is due to the greater atomic weight to unit cell volume (MW/V) ratio for  $\text{SrTa}_4\text{TiO}_{17}$  than for  $\text{SrNb}_4\text{TiO}_{17}$ .

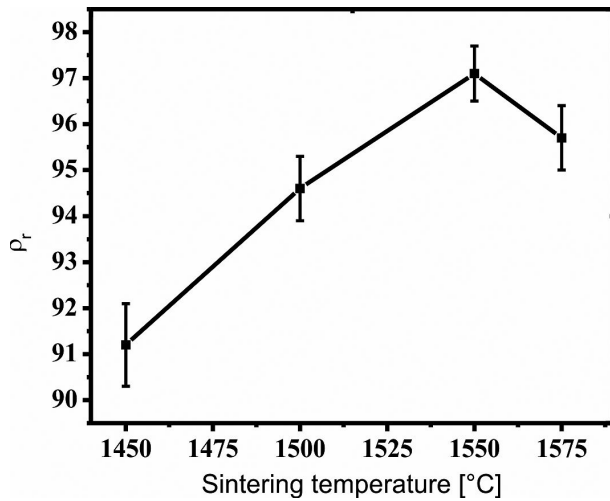


Fig. 2. Variation in  $\rho_r$  of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics with sintering temperature.

The variation in relative density  $\rho_r$  of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics as a function of increasing sintering temperature is shown in Fig. 2. The  $\rho_r$  initially increased as the sintering temperature was increased from  $1450^\circ\text{C}$  to  $1550^\circ\text{C}$  and then slightly decreased with further increase in sintering temperature to  $1575^\circ\text{C}$ . The density reached to a maximum value at  $1550^\circ\text{C}$ . The initial increase in density of the ceramics may be due to the elimination of the pores under the mechanism of grain growth. Generally, at higher temperatures abnormal grain growth occurs which causes inhomogeneous microstructure, leading to porosity. Therefore, the final decrease in density above  $1550^\circ\text{C}$  could be attributed to the abnormal grain growth.

The secondary electron microscopy (SEM) images of thermally etched Au-coated surfaces of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics sintered at  $1450^\circ\text{C}$  to  $1575^\circ\text{C}$  for 4 h are shown in Fig. 3. The microstructure is comprised of plate-like grains whose average grain size increased from  $2 \mu\text{m}$  to  $5 \mu\text{m}$  with the increase in sintering temperature from  $1450^\circ\text{C}$  to  $1575^\circ\text{C}$ . Some abnormal grain growth can also be seen at sintering temperature of  $1575^\circ\text{C}$  which is consistent with relative density data. The relative permittivity  $\epsilon_r$  of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics sintered at  $1550^\circ\text{C}$ , measured in the frequency range of 1 kHz to 1 MHz is shown in Fig. 4.  $\epsilon_r$  significantly decreased with an increase in frequency due to the reduction of active polarization mechanism at higher frequencies. At lower frequencies, the electronic, ionic, dipolar and interfacial/surface polarizations contribute to  $\epsilon_r$ , however, above 100 kHz, the contribution from the interfacial/surface polarization can no longer follow the field, resulting in a decrease in  $\epsilon_r$  from 75 to 67 [17].

The variation in microwave dielectric properties of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics with sintering temperature is shown in Fig. 5.  $\epsilon_r$  and  $Q_{uf_0}$  show the same trend with sintering temperature (Fig. 5a and Fig. 5b) as the relative density (Fig. 2). It is generally accepted that  $\epsilon_r$  of a material depends on the ionic polarizability  $\alpha_D$  of ions constituting the composition, secondary phase(s), and its density.  $\epsilon_r \sim 66$  was obtained for the sample sintered at  $1550^\circ\text{C}$ . The  $\epsilon_r$  of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  is lower and its  $Q_{uf_0}$  is higher than those of its Nb counterpart ( $\text{Sr}_5\text{Nb}_4\text{TiO}_{17}$ ) for which  $\epsilon_r \sim 74$  and  $Q_{uf_0} \sim 1303 \text{ GHz}$  were reported in a previous study [11]. Since ionic dielectric polarizability of  $\text{Ta}^{5+}$  ( $4.73 \text{ \AA}^3$ ) is larger than that of  $\text{Nb}^{5+}$  ( $3.93 \text{ \AA}^3$ ) [18], therefore, the substitution of Ta for Nb should increase  $\epsilon_r$  and reduce  $Q_{uf_0}$  value but the trend was opposite. The same trend for  $\epsilon_r$  and  $Q_{uf_0}$  value with Ta substitution for Nb was also observed in  $\text{Ca}_5\text{Nb}_{2-x}\text{Ta}_x\text{TiO}_{12}$  ( $x = 0$  to 2) [14] and  $\text{Ba}_4\text{LaTiNb}_{3-x}\text{Ta}_x\text{O}_{15}$  ceramics [12]. Ratheesh et al. [19] suggested that the larger short range interaction parameter in O–Ta–O bond in comparison to O–Nb–O results in higher quality

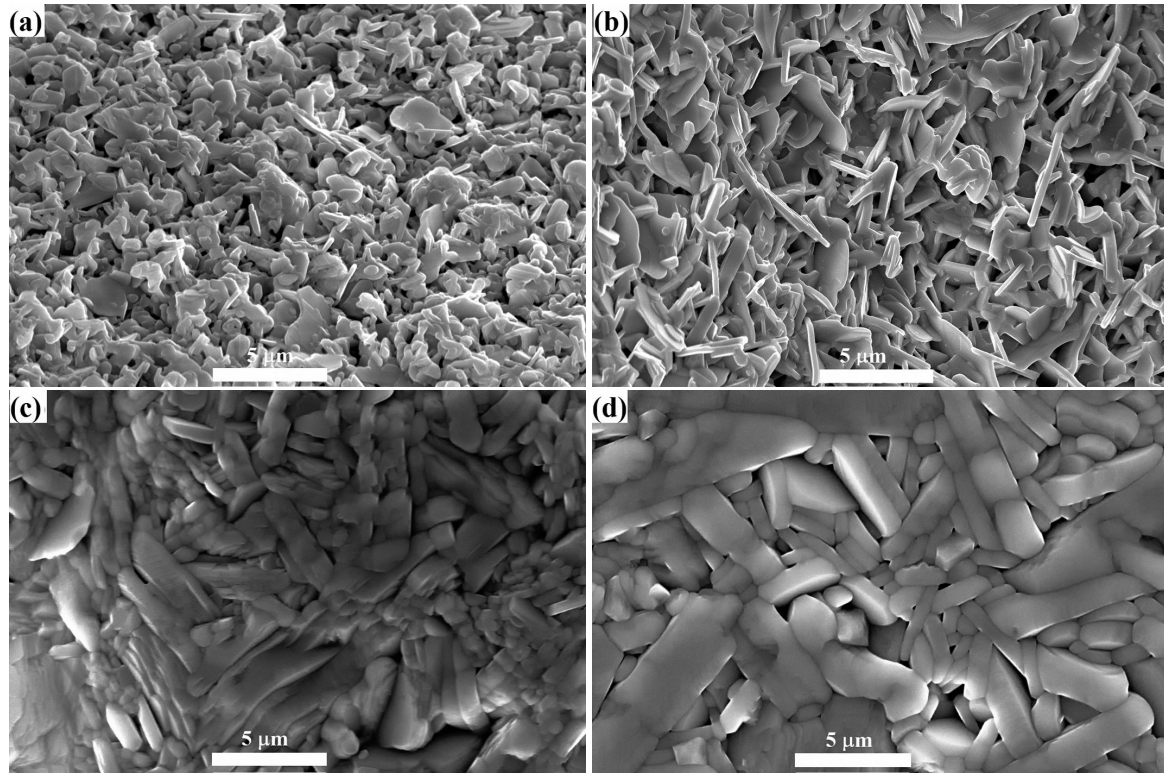


Fig. 3. Scanning electron microscopy (SEM) images of sintered and thermally etched surface of  $\text{Sr}_5\text{Ta}_4\text{Ti}_4\text{O}_{17}$  ceramics prepared at (a) 1450 °C, (b) 1500 °C, (c) 1550 °C and (d) 1575 °C.

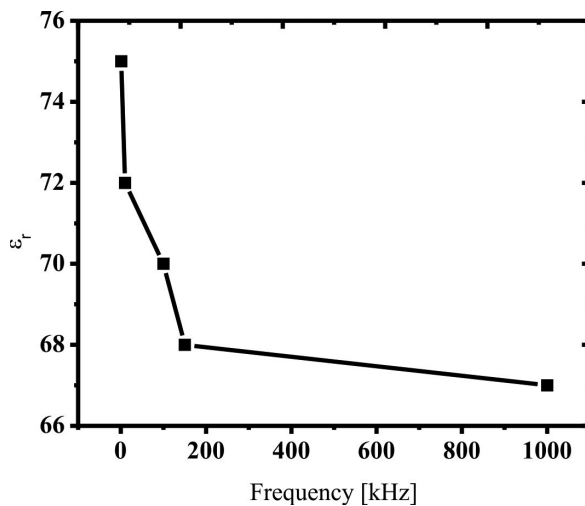


Fig. 4. Variation in  $\epsilon_r$  of  $\text{Sr}_5\text{Ta}_4\text{Ti}_4\text{O}_{17}$  ceramics as a function of frequency.

factor and lower  $\epsilon_r$  and therefore, this suggestion could explain the results in the present study. The quality factor  $Q$  or its inverse – the dielectric

loss – is considered as the figure of merit for measuring the performance or quality of a resonator. Intrinsic and extrinsic losses contribute to the total dielectric loss of a material. The intrinsic losses are the losses that originate from the interaction of AC electric field with the phonon of the lattice which totally depends on the crystal structure. During this process, the AC electric field modifies the equilibrium state of the lattice phonons leading to energy dissipation and hence dielectric loss. The intrinsic loss is caused by defects such as grain boundaries, stacking faults, chemical or structural disorders, point defects, planar defects, line defects, inclusions, secondary phases, twinning, porosity, etc. [20].  $\tau_f \sim 180$  ppm/°C was obtained for  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics (Fig. 5c) sintered at 1550 °C which is lower than that of  $\text{Sr}_5\text{Nb}_4\text{TiO}_{17}$  ( $\sim 332$  ppm/°C) [11]. Since  $\text{Nb}^{5+}$  and  $\text{Ta}^{5+}$  have the same ionic radii (0.64 Å) [17], therefore, they will have the same tolerance factor. Thus, the effect of tolerance factor on the variation in  $\tau_f$  can



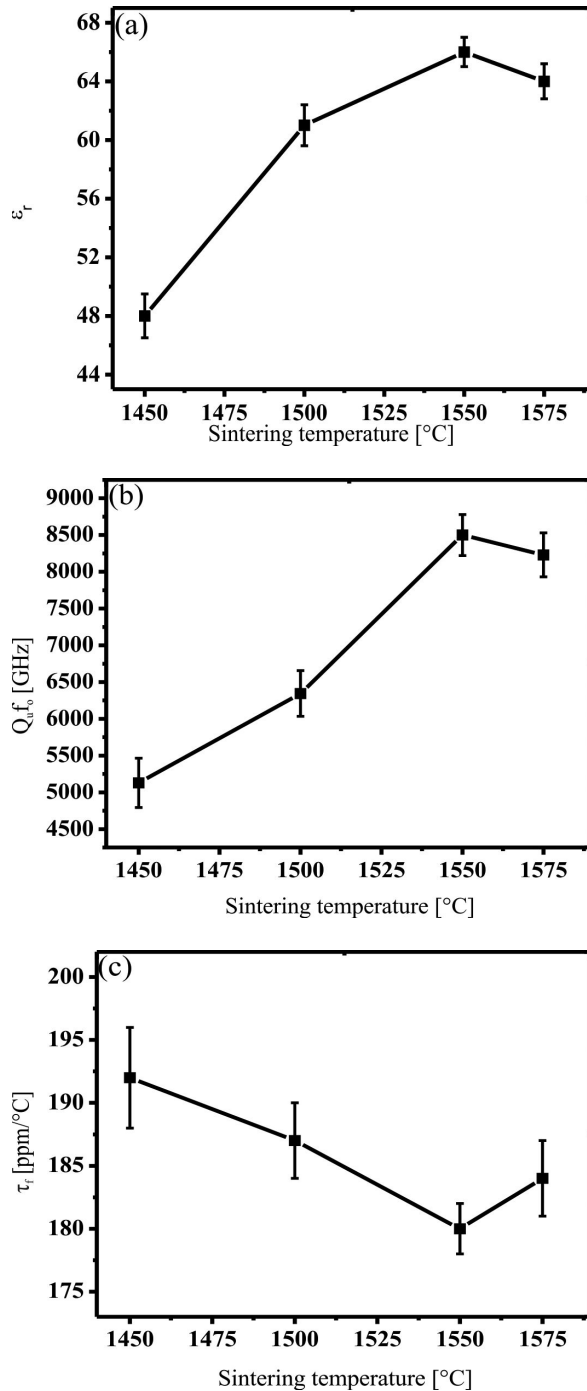


Fig. 5. Variation in (a)  $\epsilon_r$ , (b)  $Q_u f_o$ , and (c)  $\tau_f$  of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics as a function of sintering temperature.

be ignored as suggested by Reaney et al. [21]. The lower value of  $\tau_f$  of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  than that of  $\text{Sr}_5\text{Nb}_4\text{TiO}_{17}$  could be the result of relationship

Table 1. Preparation conditions, relative densities and microwave dielectric properties of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics sintered at different temperatures.

S.T [°C]	$\rho_r$	$\epsilon_r$	$Q_u f_o$ [GHz]	$\tau_f$ [ppm/°C]
1450	91.2±0.9	48±1.5	5130±345	192±8.0
1500	94.6±0.7	61±1.4	6345±310	187±6
1550	97.1±0.6	66±1.0	8500±280	180±5
1575	95.7±0.7	64±1.2	8230±300	184±6

between  $\tau_c$  and  $\tau_f$  [22]. The processing conditions and the properties of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  are also summarized in Table 1. Further work to reduce the  $\tau_f$  is in progress and hence, improvement in the  $Q_u f_o$  values of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics for possible microwave applications can be expected.

## 4. Conclusions

Single phase, >95 % dense  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics was prepared by sintering at 1550 °C for 4 h. Optimum microwave dielectric properties i.e.  $\epsilon_r \sim 66$ ,  $Q_u f_o \sim 8500$  GHz and  $\tau_f \sim 180$  ppm/°C were achieved for  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics sintered at 1550 °C for 4 h. Further work is in progress to tune the  $\tau_f$  to zero to further improve the  $Q_u f_o$  values of  $\text{Sr}_5\text{Ta}_4\text{TiO}_{17}$  ceramics by some suitable cation substitution.

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